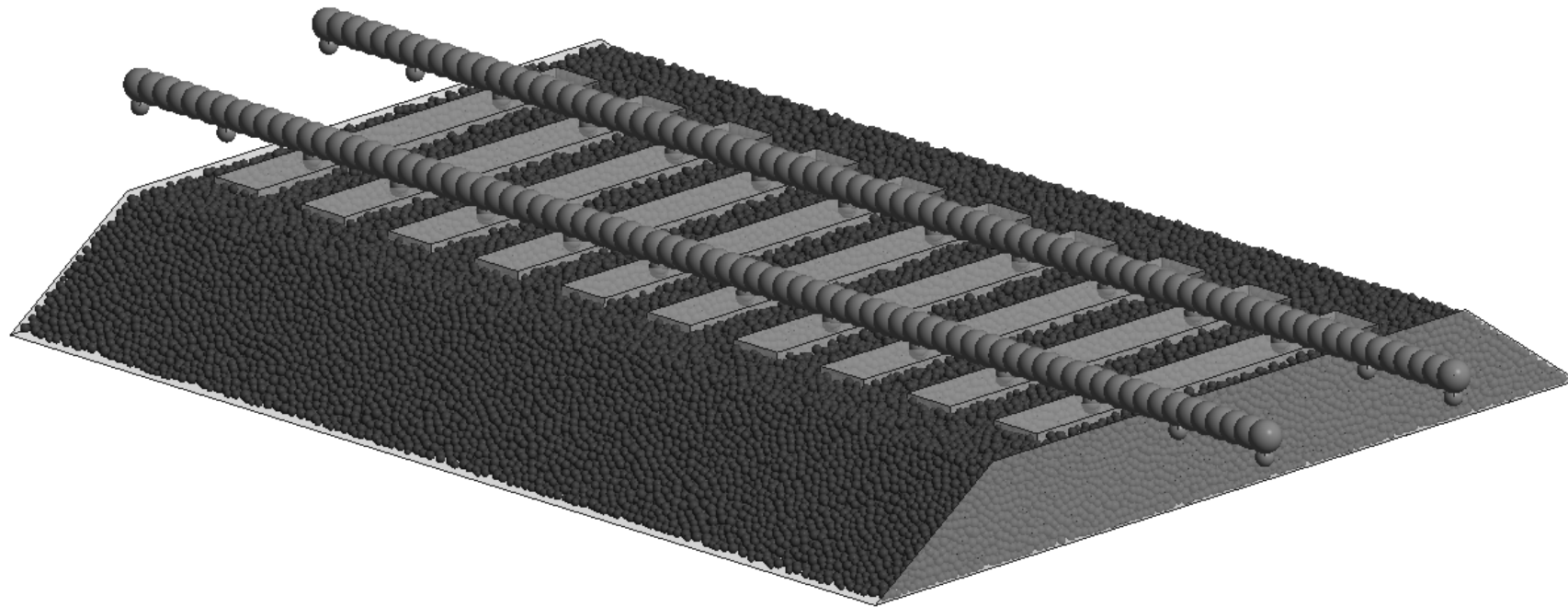


# Full-scale numerical calculation of ballasted tracks with the Discrete Element Method



Joaquín Irazábal, Fernando Salazar and Eugenio Oñate

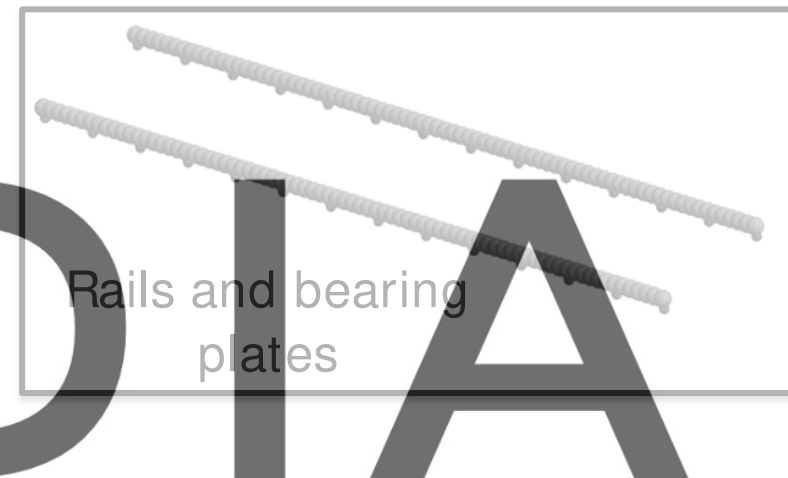
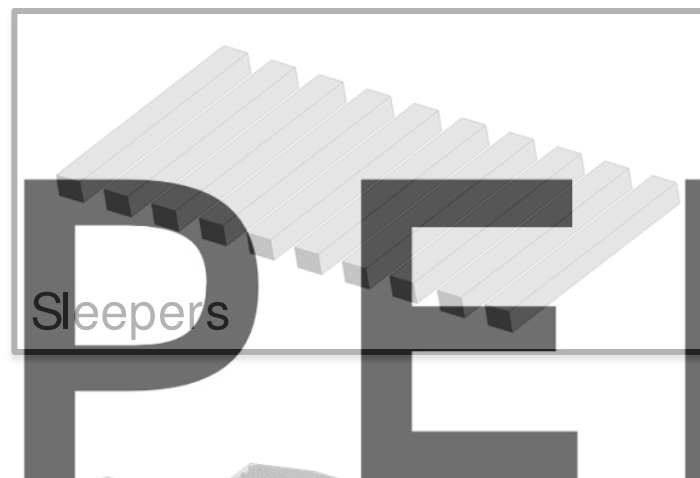
# SCIPEDIA



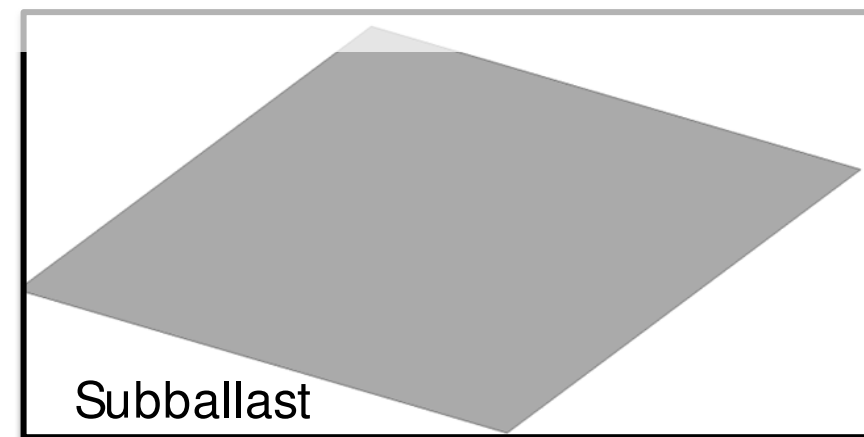
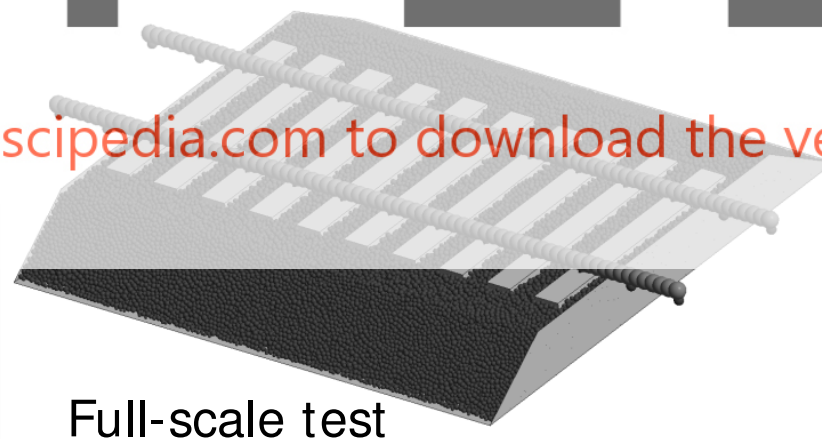
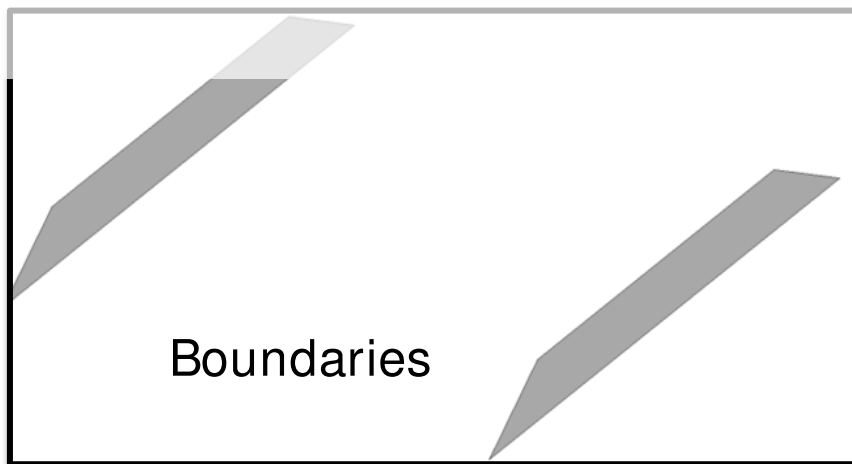
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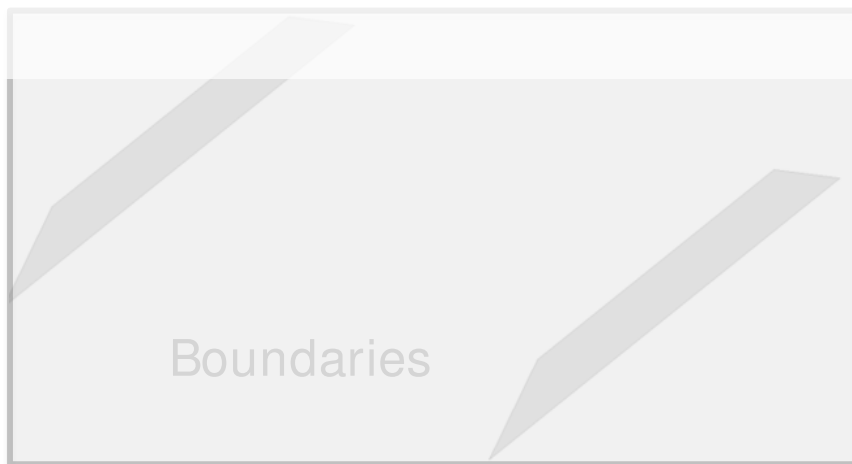
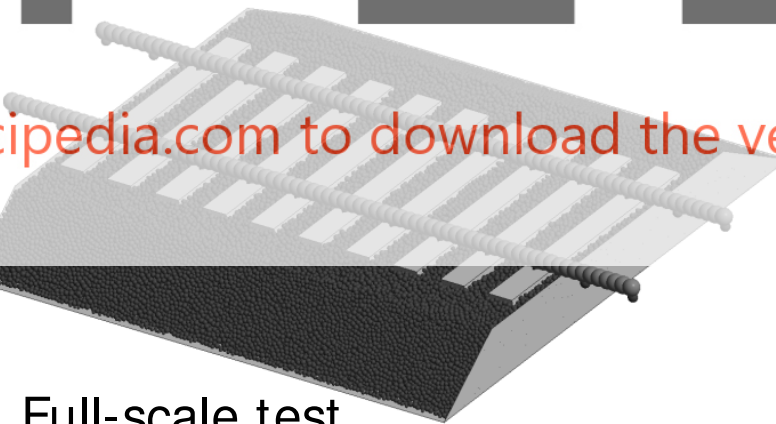
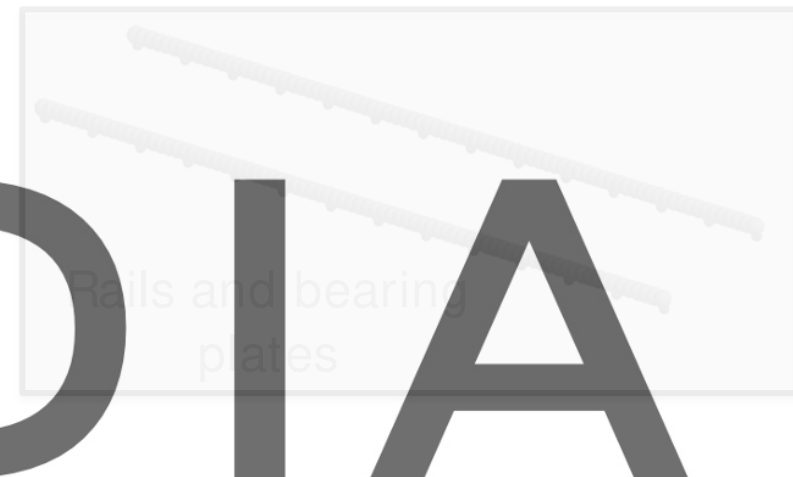
<https://github.com/KratosMultiphysics/Kratos>  
<http://gid.cimne.upc.es/>



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Ballast | Sleepers | Rails, bearing plates | Boundary walls | Subballast |  
 | Full scale railway track tests | Summary and ongoing work

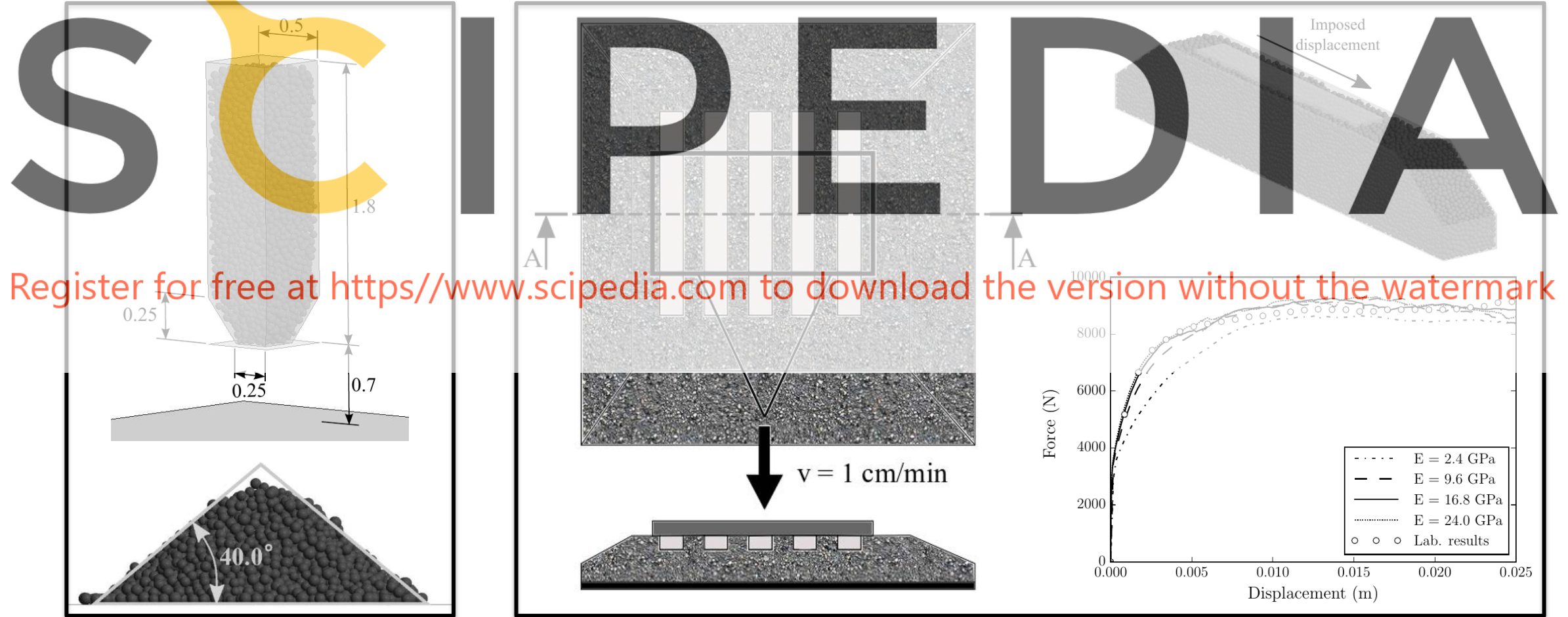


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**Ballast** | Sleepers | Rails, bearing plates | Boundary walls | Subballast |  
| Full scale railway track tests | Summary and ongoing work



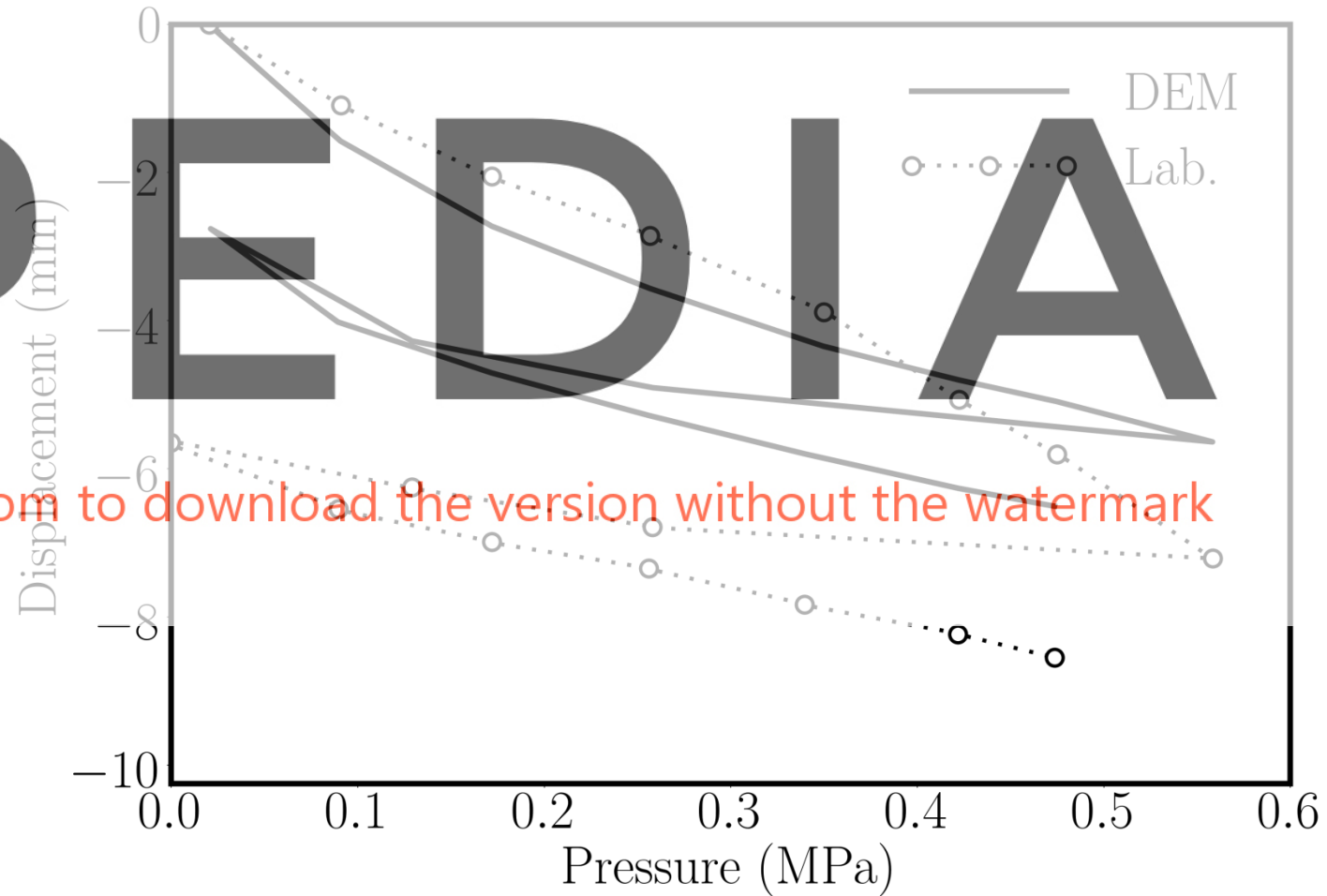
Good results applying the Hertz-Mindlin contact model



**Ballast** | Sleepers | Rails, bearing plates | Boundary walls | Subballast |  
| Full scale railway track tests | Summary and ongoing work



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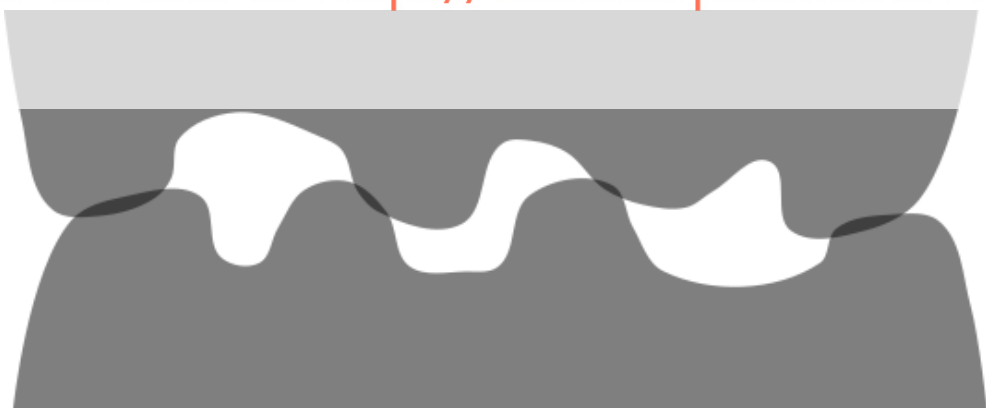


Paderno C. Simulation of ballast behaviour under traffic and tamping process. PhD Thesis 2009.

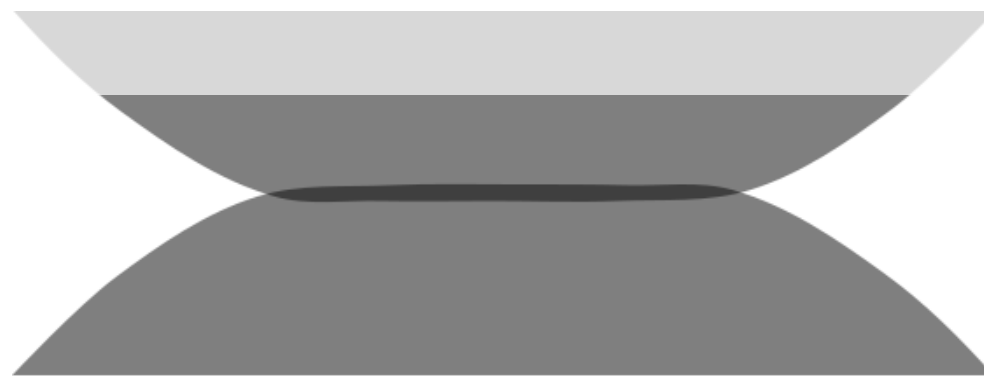
Hertzian contact model: contact stiffness depends on the contact volumen but does not take into account edge breakage

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Real contact geometry

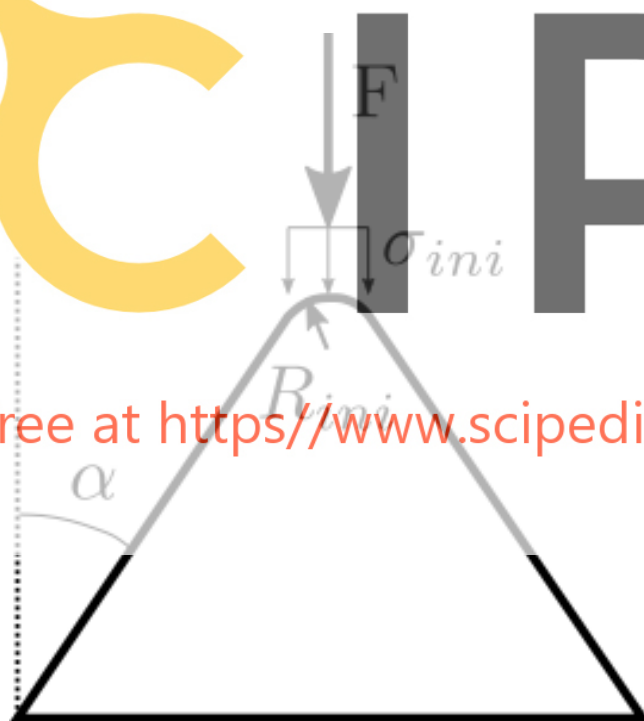


Numerical contact geometry

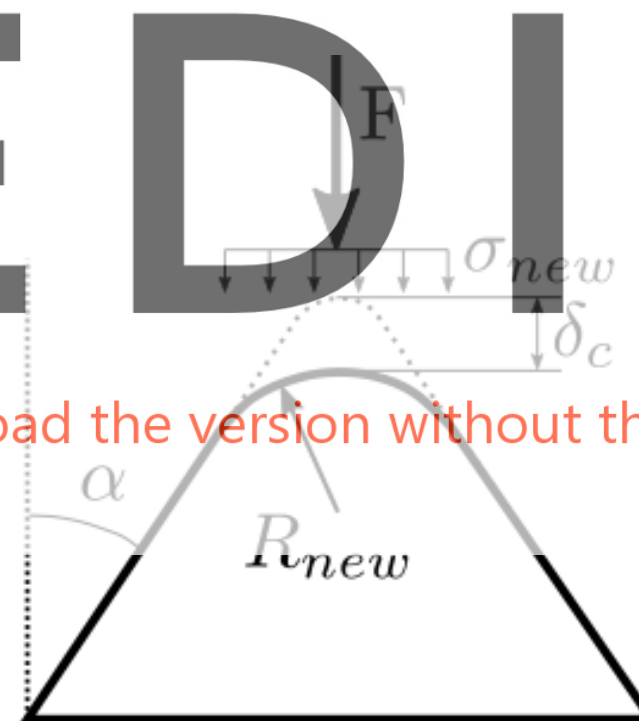
Conical damage contact model: accounts for edge breakage  
Two new material properties to define: Maximum stress and  $\alpha$

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Initial radius



Final Radius and offset

Harkness, J., Zervos, A., Le Pen, L., Aingaran, S., & Powrie, W. (2016). Discrete element simulation of railway ballast: modelling cell pressure effects in triaxial tests. Granular Matter, 18(3), 65.

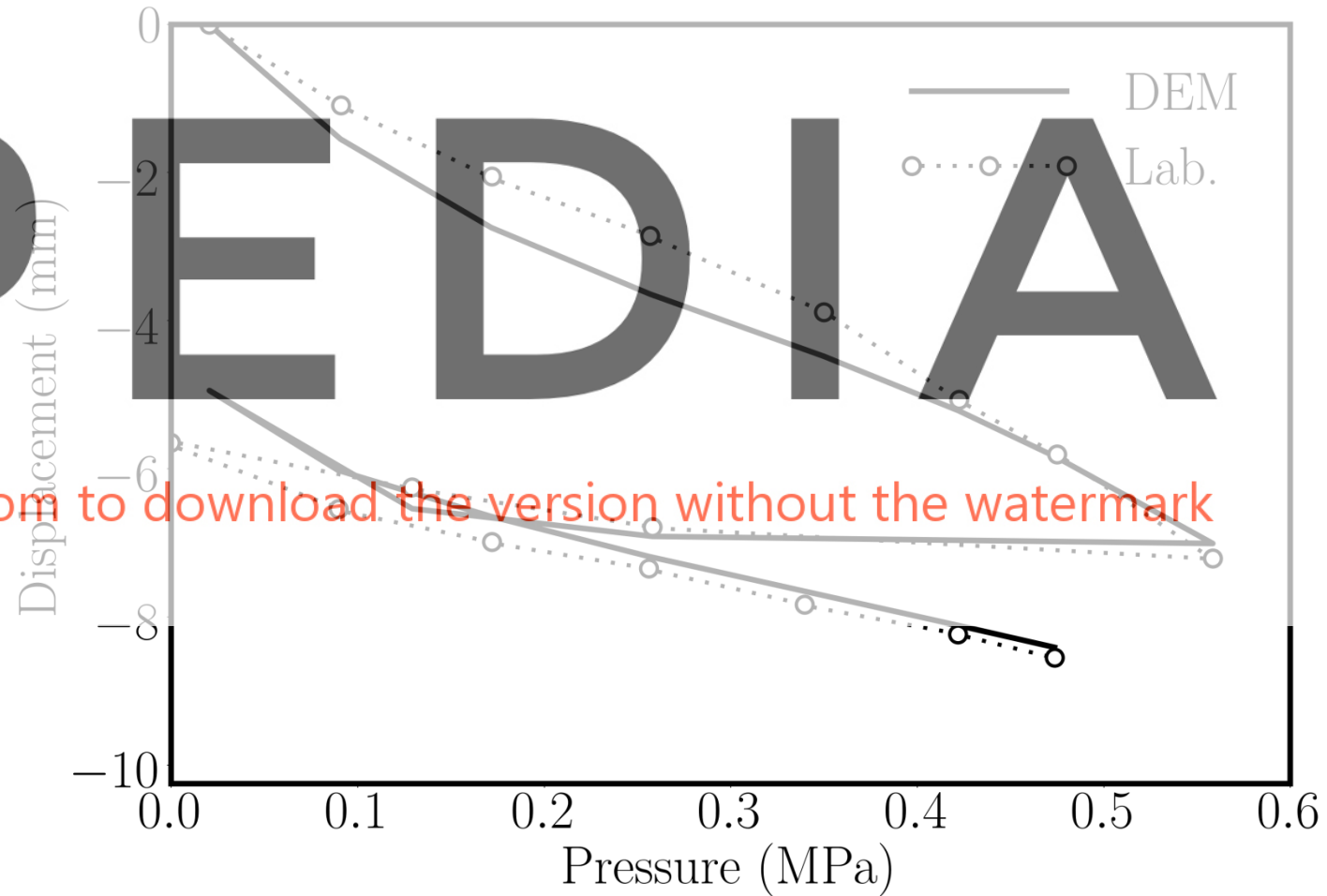
**Ballast** | Sleepers | Rails, bearing plates | Boundary walls | Subballast |  
| Full scale railway track tests | Summary and ongoing work



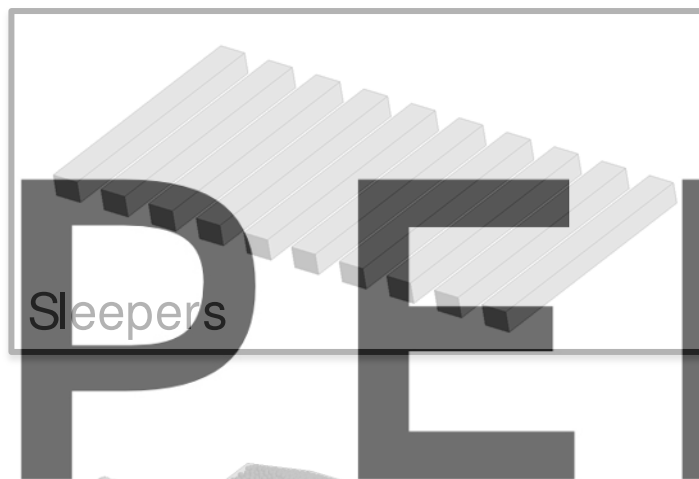
$\sigma_{max} = 500$  MPa  
 $\alpha = 89.4$  degrees



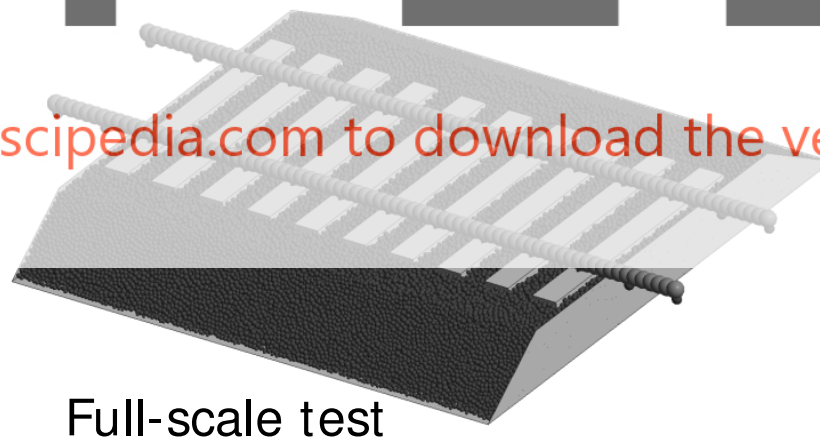
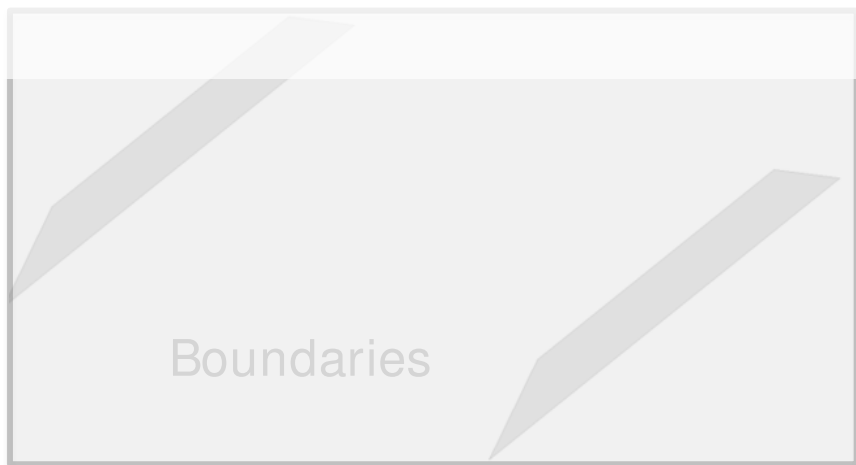
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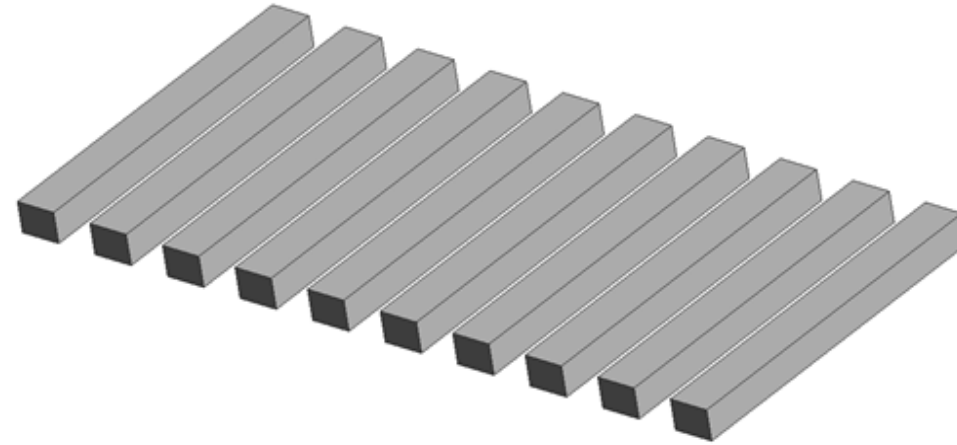


Paderno C. Simulation of ballast behaviour under traffic and tamping process. PhD Thesis 2009.



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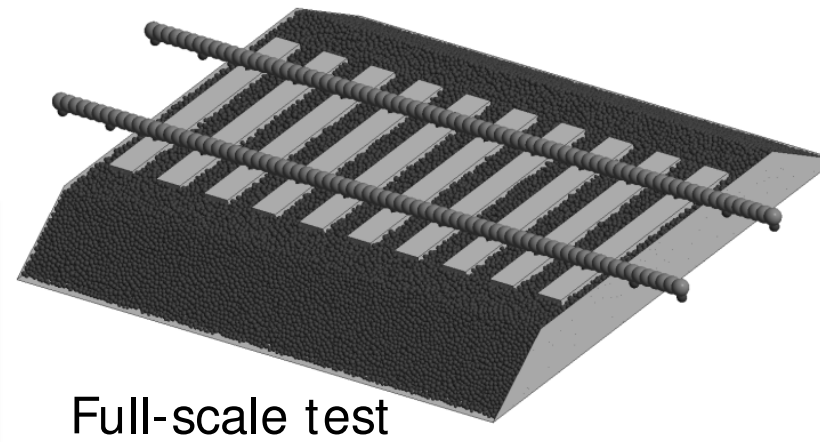
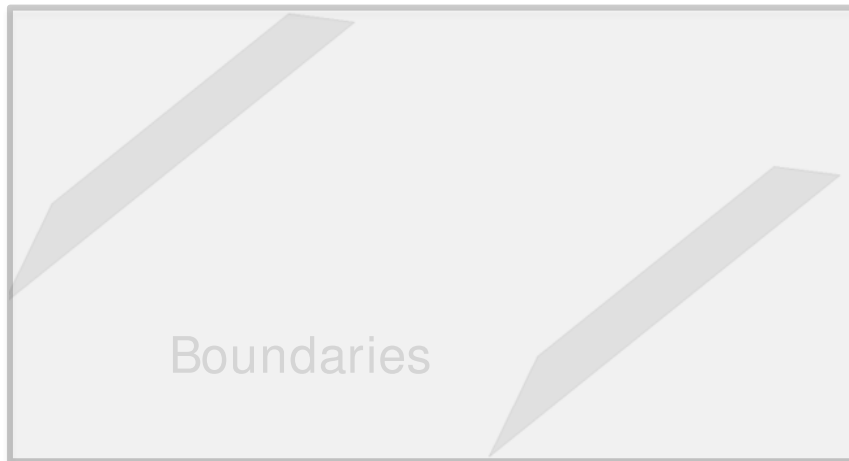
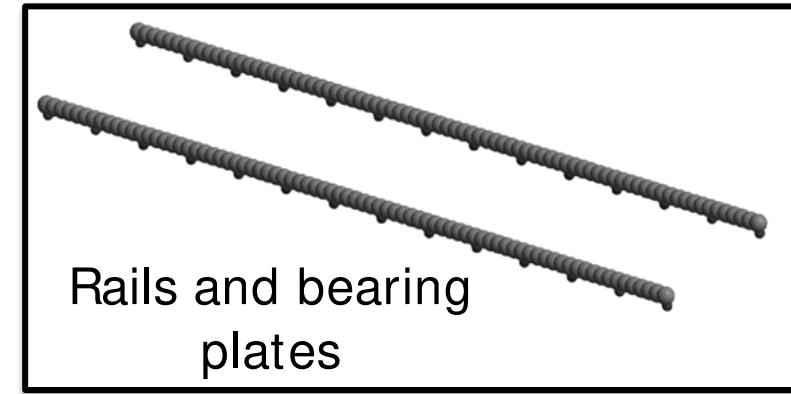
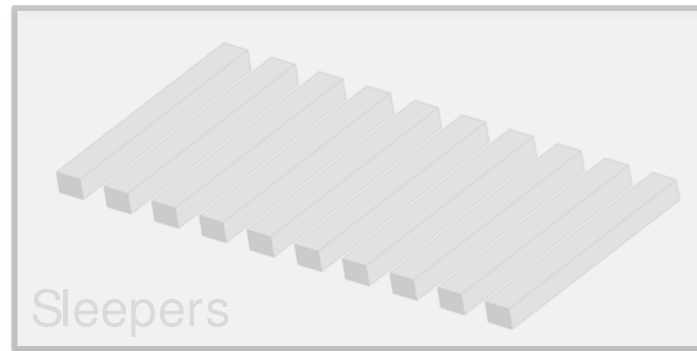
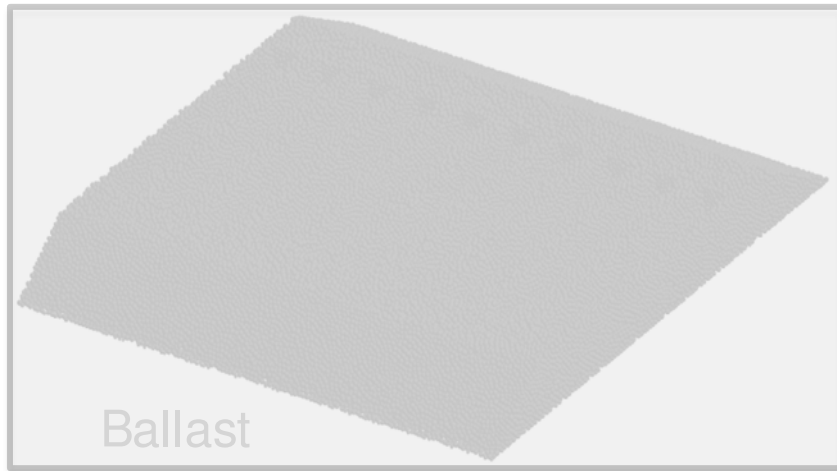
Rigid bodies and simplified geometry

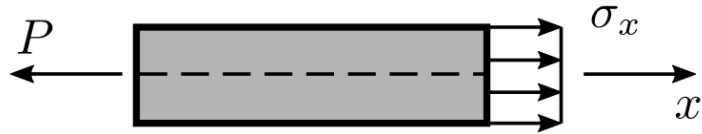
### **Sleepers contact parameters**

Young modulus = 30 Gpa (prestressed concrete)

Friction coefficient = 0.7247\*

\* Zand, J. van't, & Moraal, J. (1997) Roads and Railways Research Laboratory Technical University of Delft

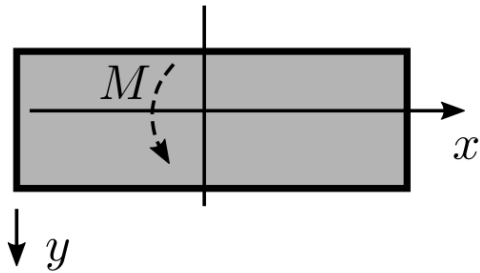




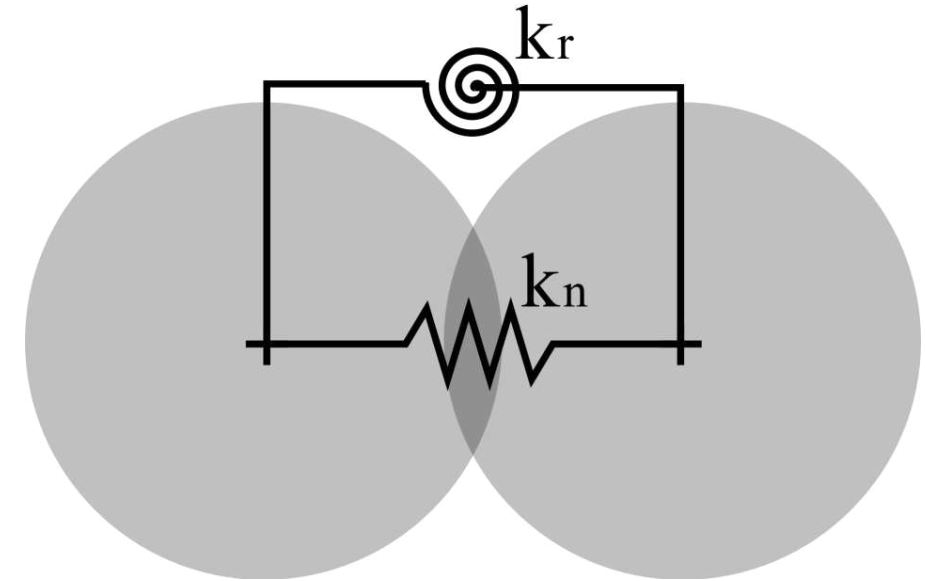
Axial loading:  $\sigma_x = \frac{P}{A}$



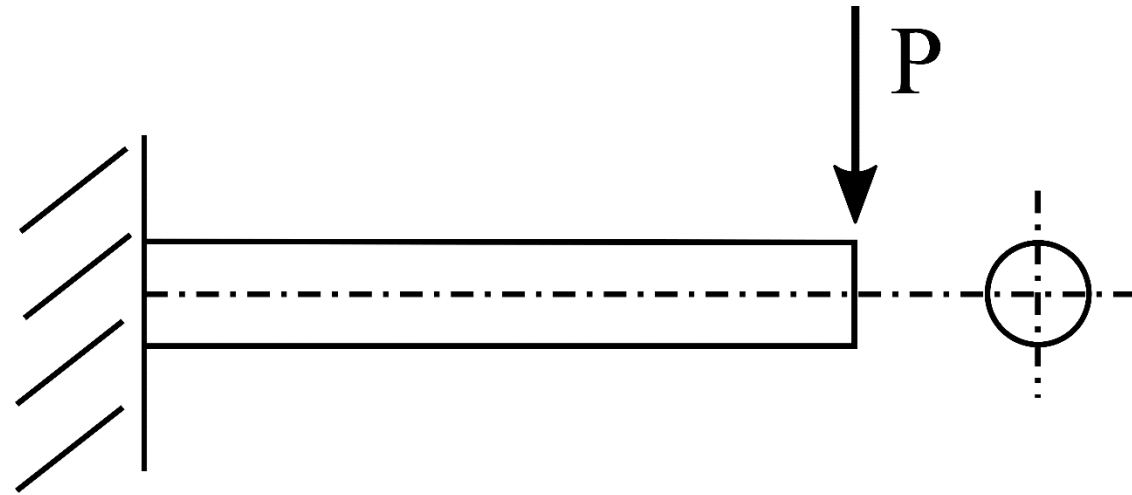
Torsion:  $\tau = \frac{T\rho}{J}$



Bending:  $\sigma_x = -\frac{My}{I}$

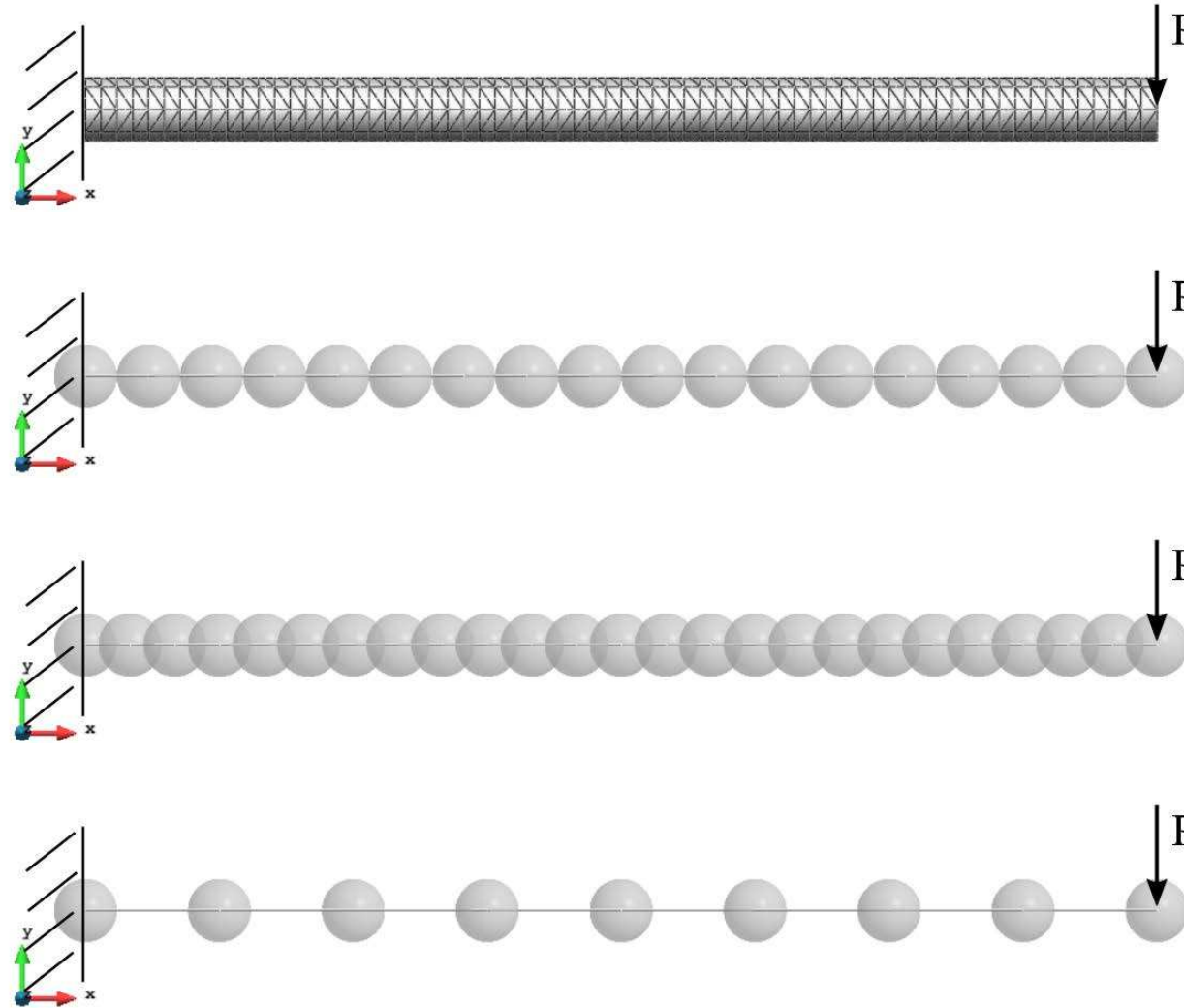






Large deformations  
 Non-linear problem

} Analytical solution unknown  $\Rightarrow$  FEM



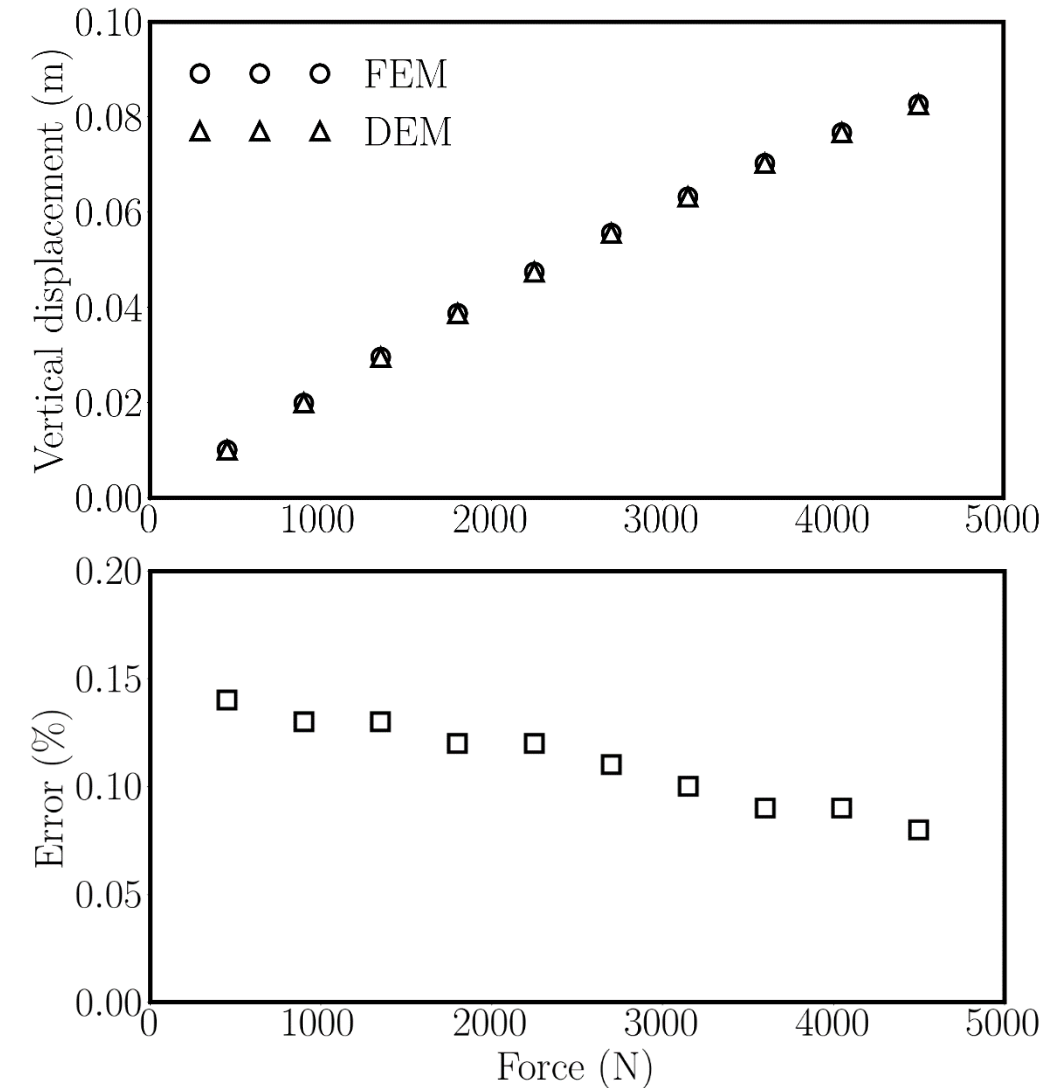
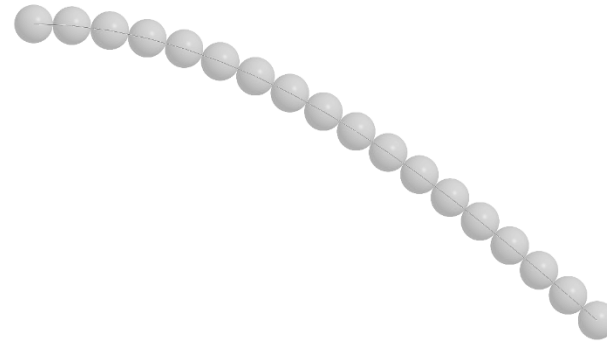
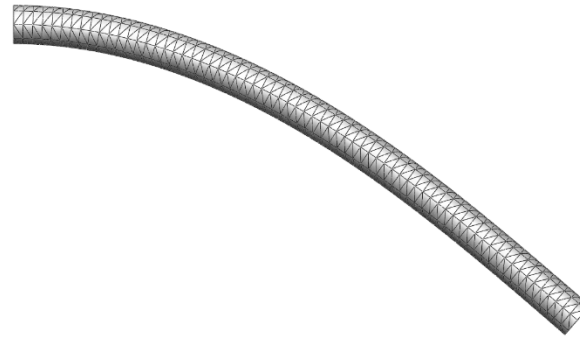
Ballast | **Sleepers** | Rails, bearing plates | Boundary walls | Subballast |  
 | Full scale railway track tests | Summary and ongoing work

$E = 117.21 \text{ GPa}$ ,  $\nu = 0.35$ ,  
 $L = 0.204 \text{ m}$  and  $R = 0.006 \text{ m}$

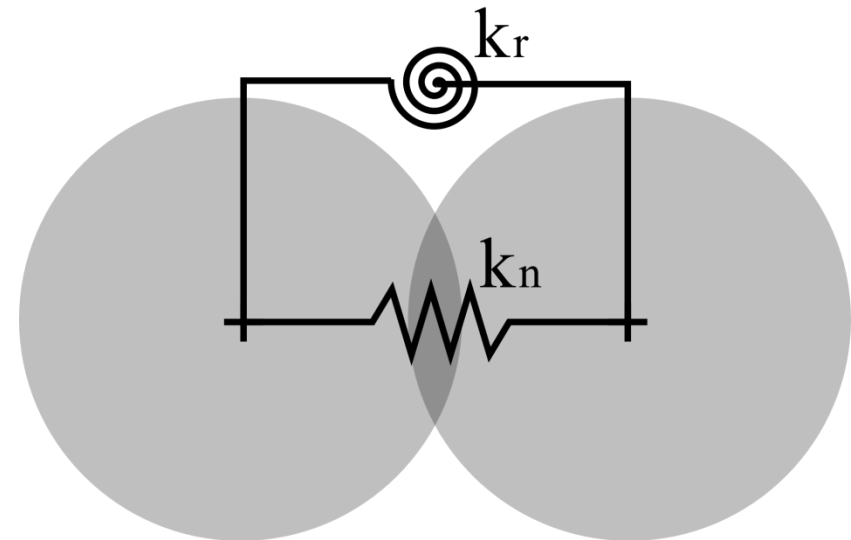
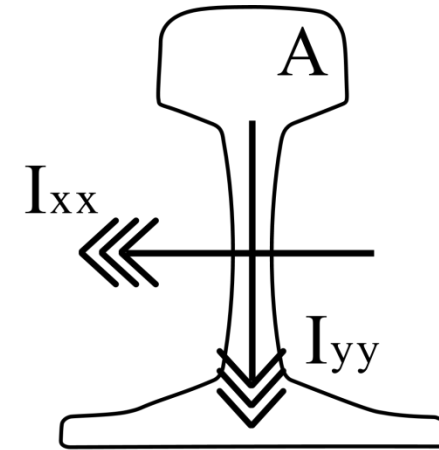
$P = 450 \text{ N}$



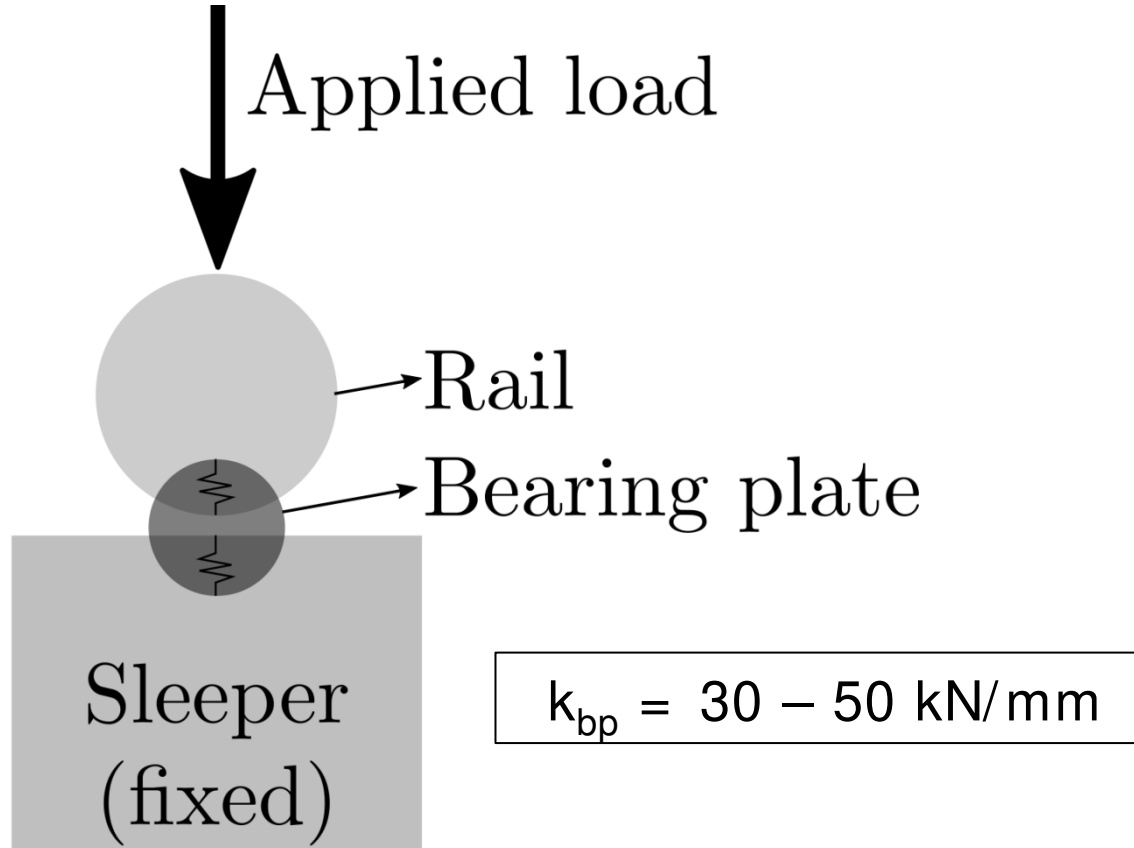
$P = 4500 \text{ N}$



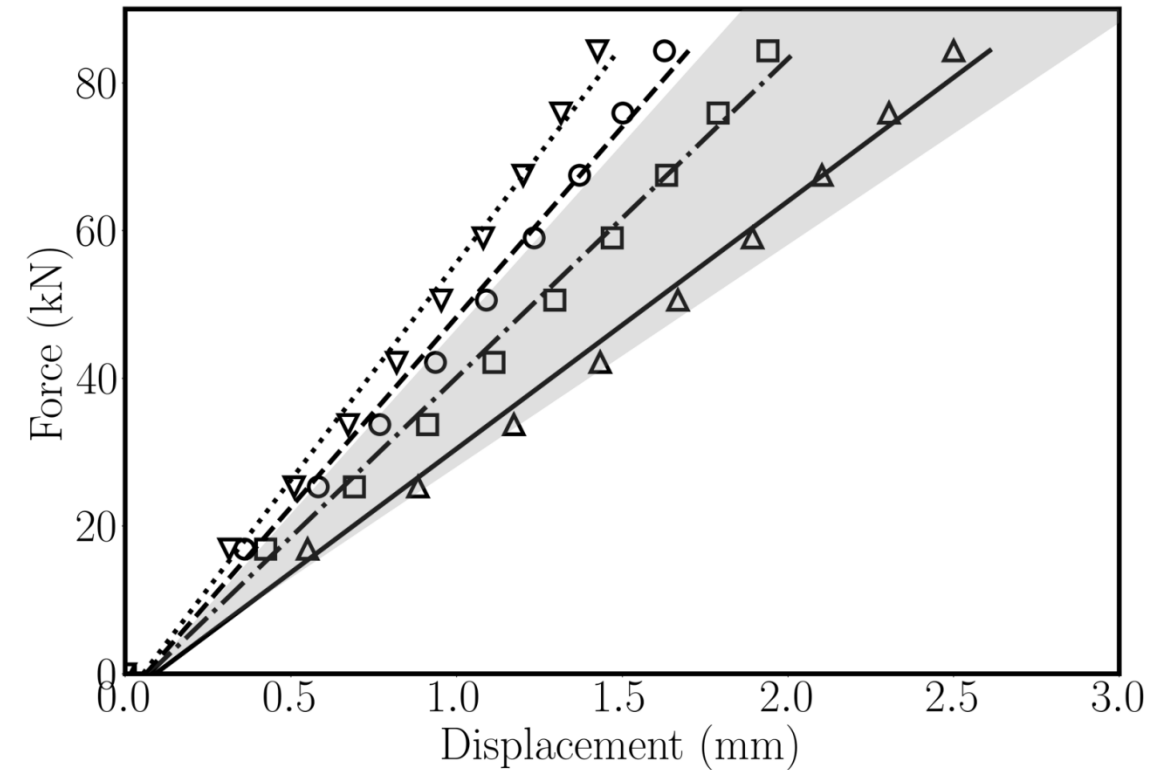
Ballast | **Sleepers** | Rails, bearing plates | Boundary walls | Subballast |  
 | Full scale railway track tests | Summary and ongoing work



Ballast | **Sleepers** | Rails, bearing plates | Boundary walls | Subballast |  
 | Full scale railway track tests | Summary and ongoing work

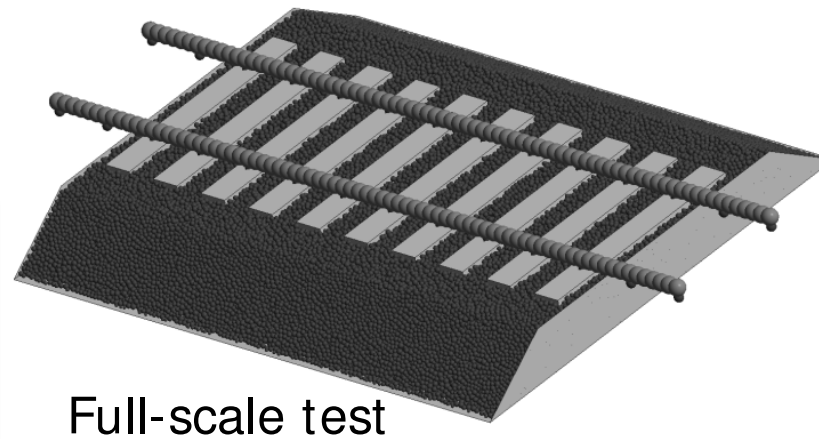
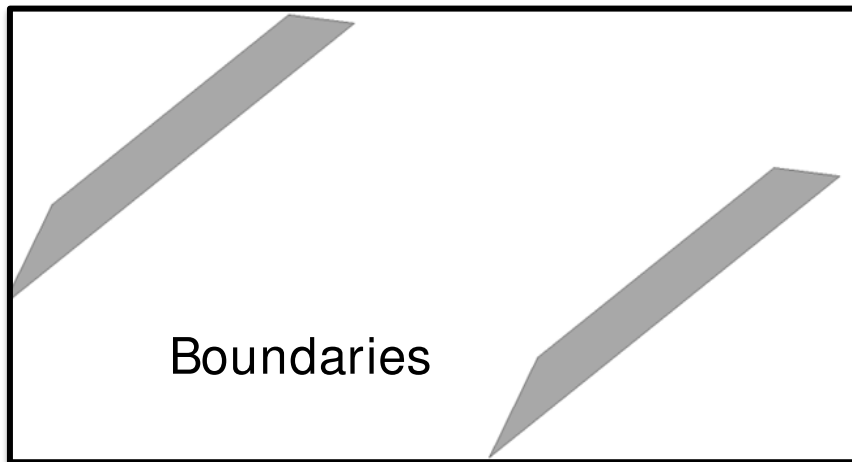
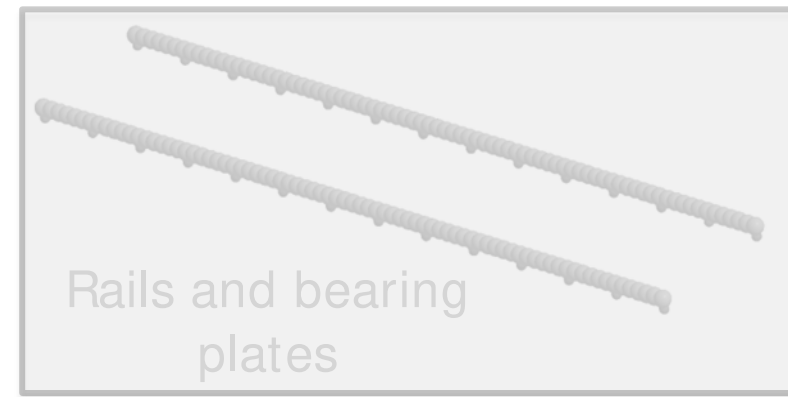
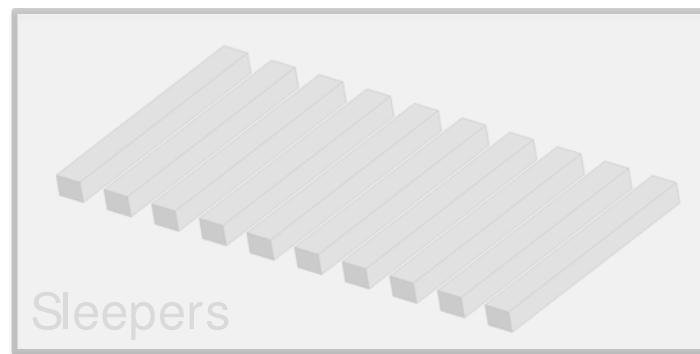
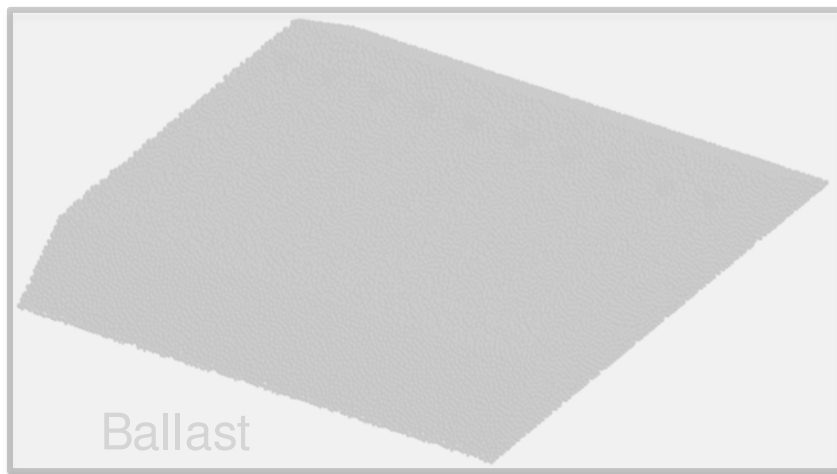


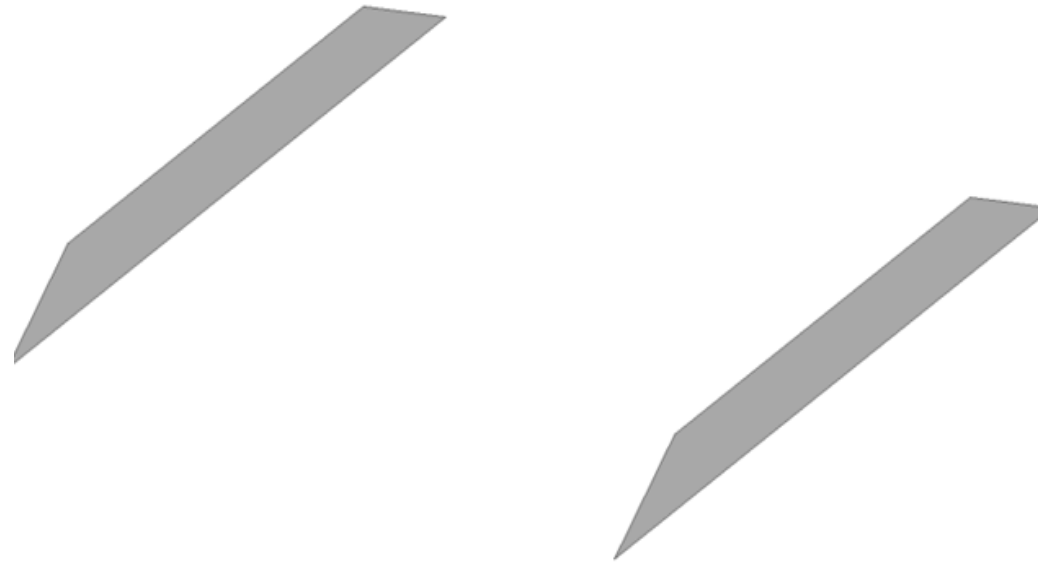
$\Delta$	$\Delta$	$E_{bp} = 2 \text{ GPa}$	—	$k_{bp} = 33.51 \text{ kN/mm}$
$\square$	$\square$	$E_{bp} = 3 \text{ GPa}$	-.-	$k_{bp} = 43.18 \text{ kN/mm}$
$\circ$	$\circ$	$E_{bp} = 4 \text{ GPa}$	---	$k_{bp} = 51.50 \text{ kN/mm}$
$\nabla$	$\nabla$	$E_{bp} = 5 \text{ GPa}$	.....	$k_{bp} = 58.81 \text{ kN/mm}$



Pita, A. L., Teixeira, P. F., & Robusté, F. (2004). High speed and track deterioration: the role of vertical stiffness of the track. Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit, 218(1), 31-40.





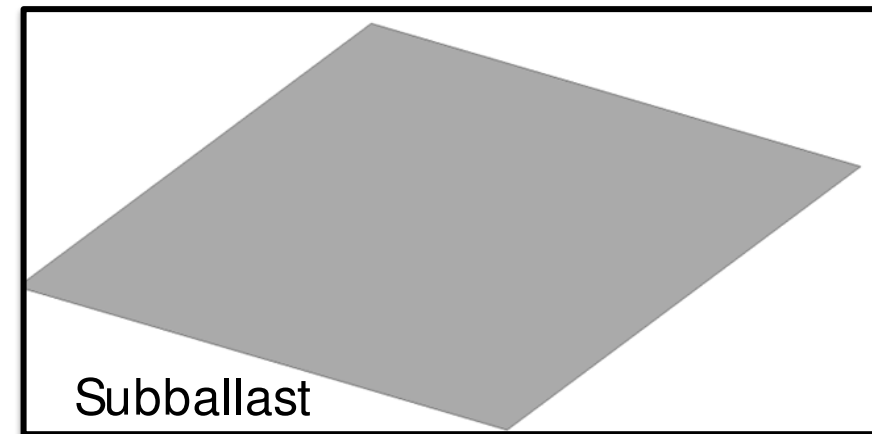
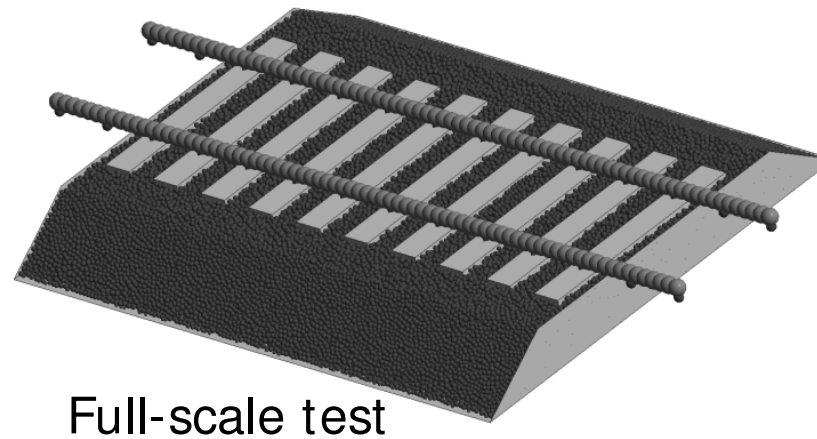
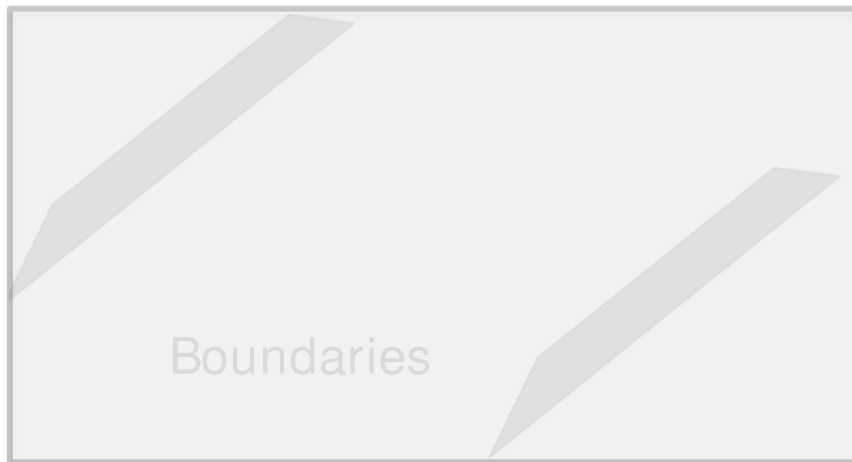
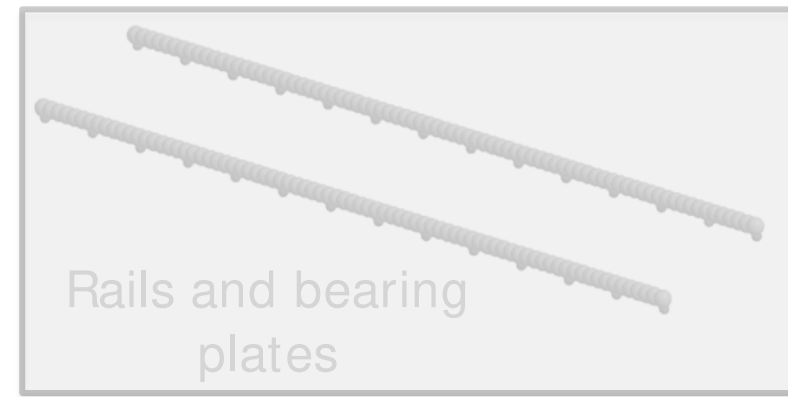
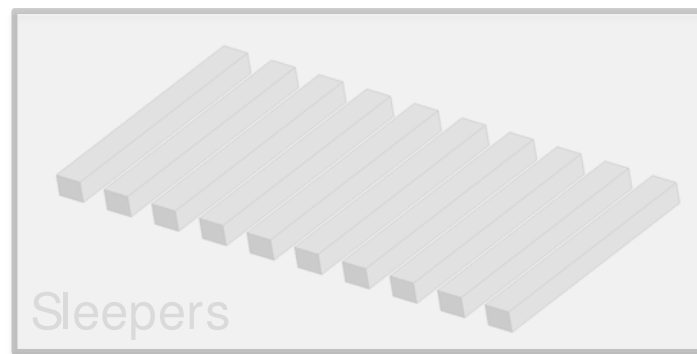
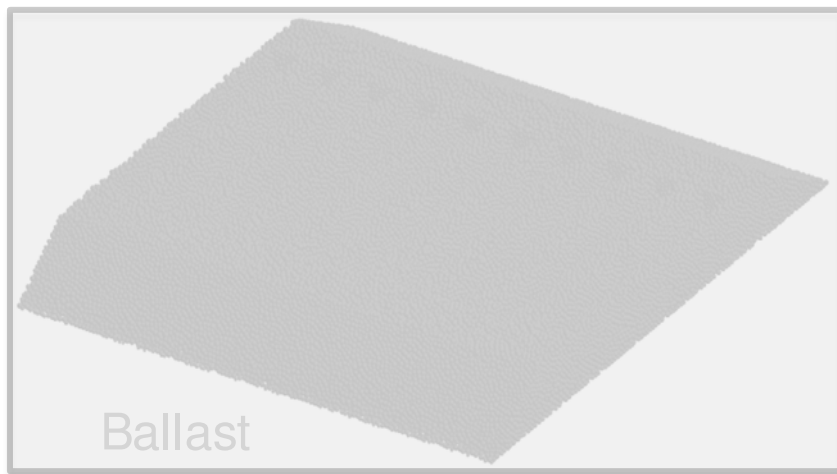


## Contact between ballast and boundary walls

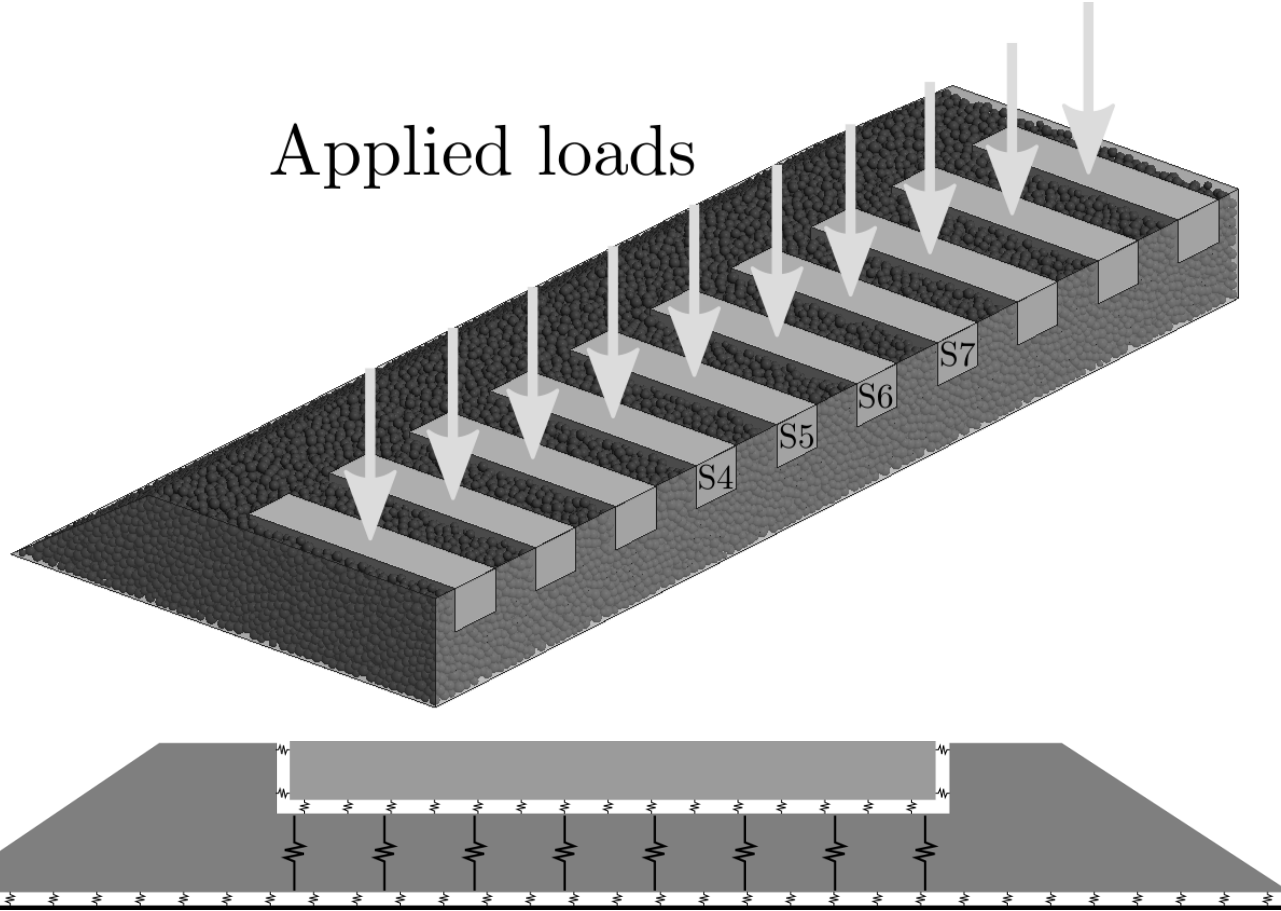
Young modulus = 200 Mpa\*

Friction coefficient = 0.0 (“mirrored particles”)

\* Paderno, C. Simulation of ballast behaviour under traffic and tamping process. 9<sup>th</sup> Swiss Transport Research Conference. 2009.

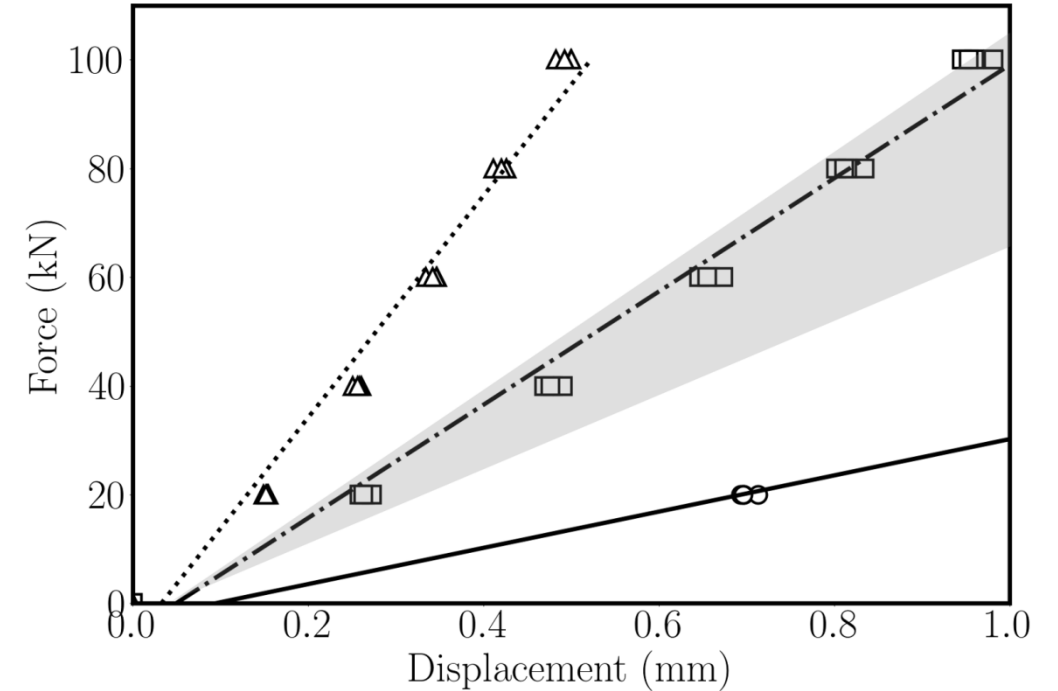


Applied loads

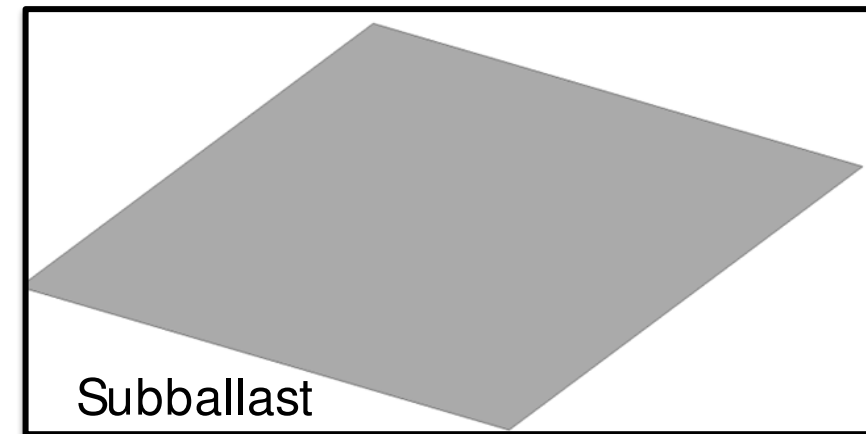
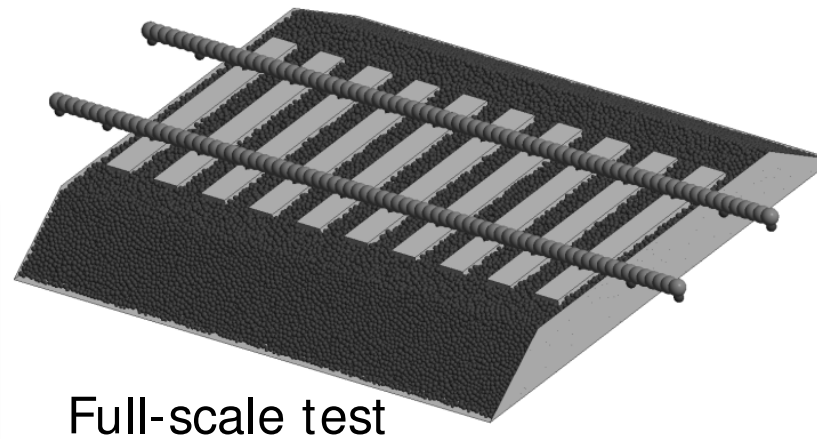
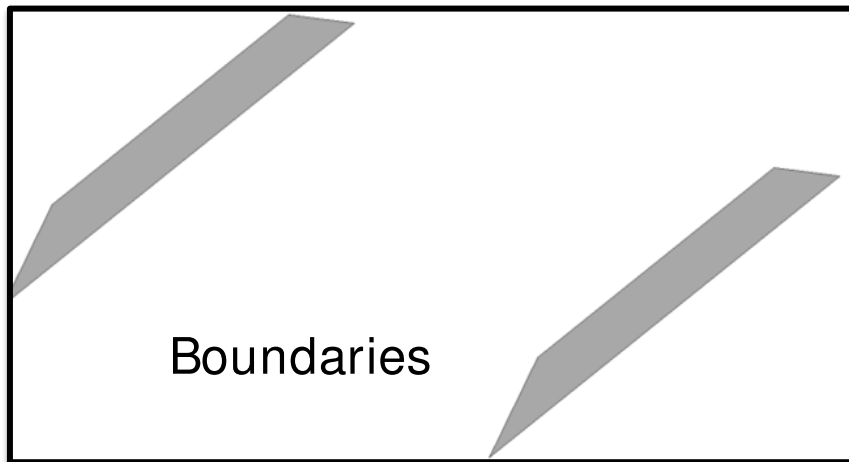
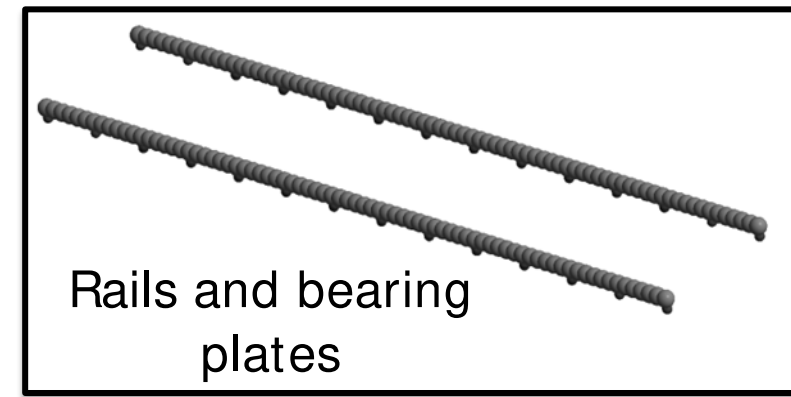
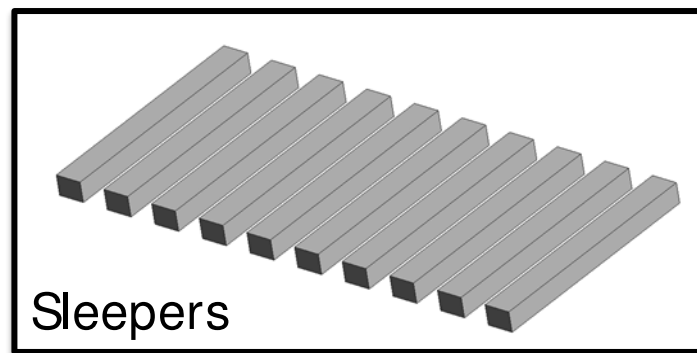
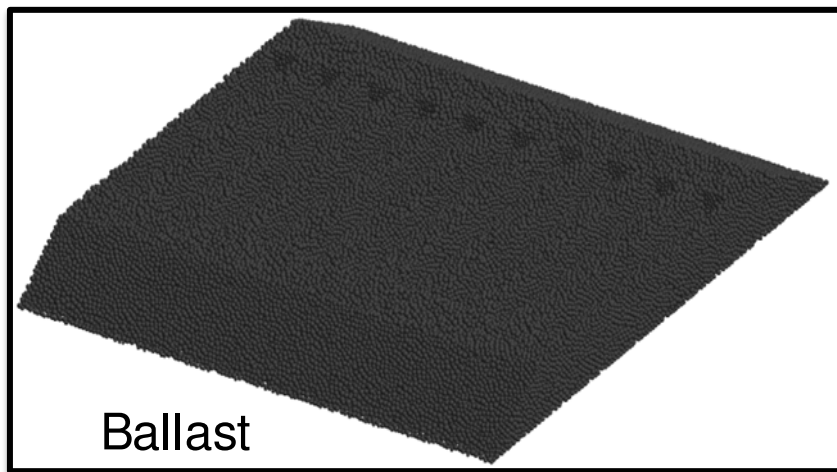


$$k_{sub} = 70 - 110 \text{ kN/mm}$$

○ ○	$E_{sub} = 3 \text{ MPa}$	—	$k_{sub} = 33.34 \text{ kN/mm}$
□ □	$E_{sub} = 30 \text{ MPa}$	- - -	$k_{sub} = 104.17 \text{ kN/mm}$
△ △	$E_{sub} = 300 \text{ MPa}$	.....	$k_{sub} = 204.14 \text{ kN/mm}$

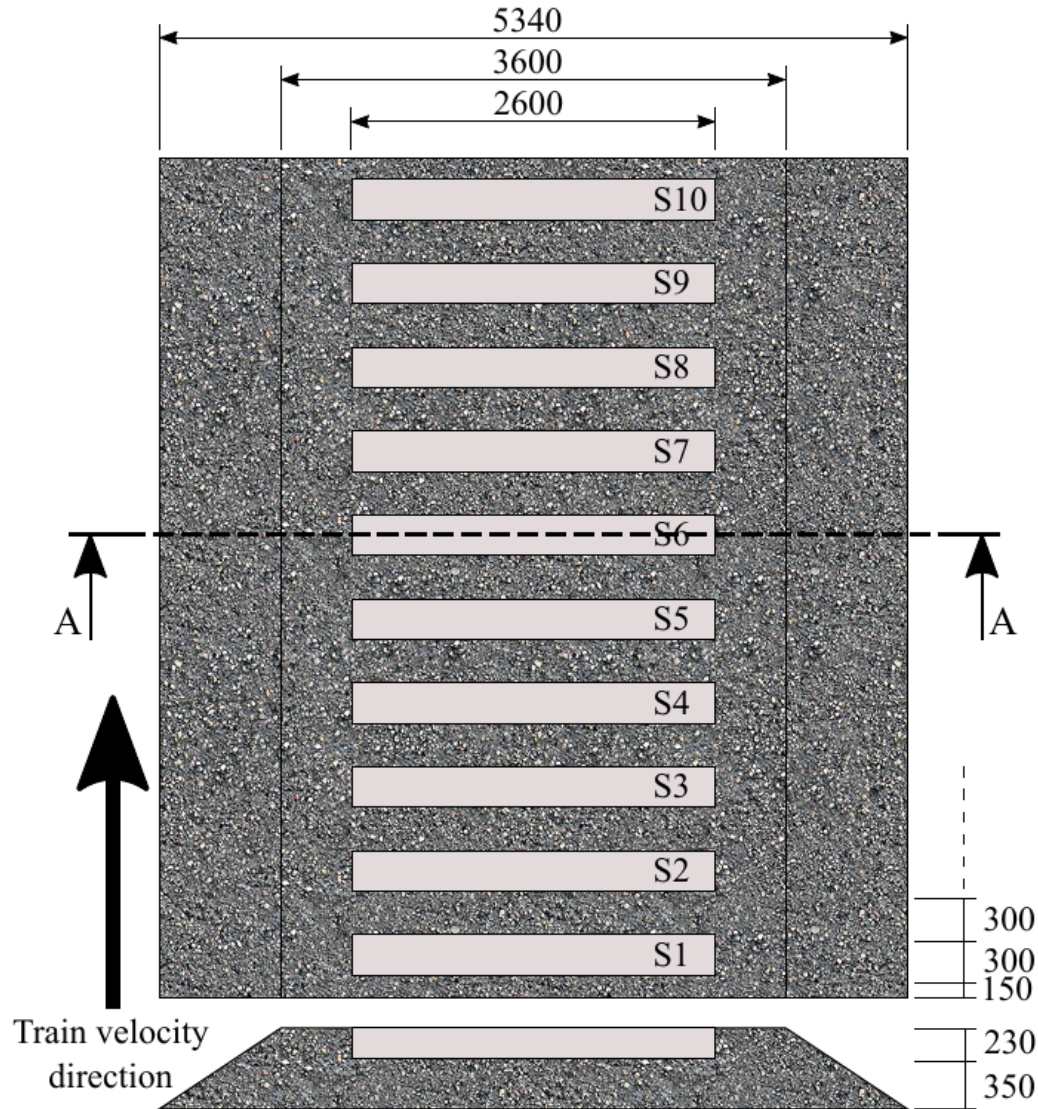


Pita, A. L., Teixeira, P. F., & Robusté, F. (2004). High speed and track deterioration: the role of vertical stiffness of the track. Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit, 218(1), 31-40.



Ballast | Sleepers | Rails, bearing plates | Boundary walls | Subballast |  
**Full scale railway track tests** | Summary and ongoing work





- Scenario 1: Well compacted track
- Scenario 2: Poorly compacted track
- Scenario 3: Fouled track (less friction\* and larger contact volume between particles)

\*Huang, H. & Tutumluer, E. (2011). Discrete Element Modeling for fouled railroad ballast. Construction and Building Materials, 25 (8) 3306–3312.



$$Q = 168732 \text{ N}$$

$$v = 250 \text{ km/h}$$

$$R = 4000 \text{ m}$$

$$A = 77.45 \text{ cm}^2$$

$$I_{xx} = 3217 \text{ cm}^4$$

$$I_{yy} = 524 \text{ cm}^4$$

Axle load

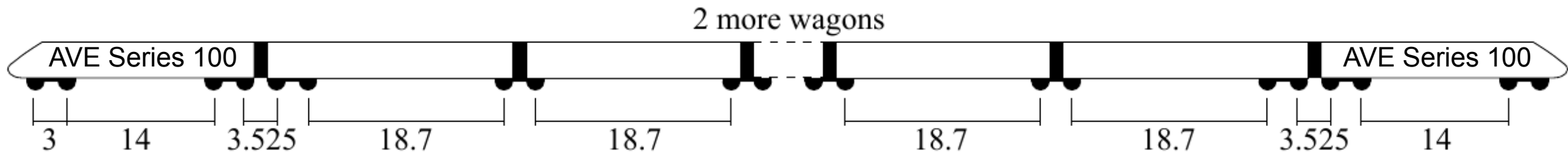
Velocity of the train

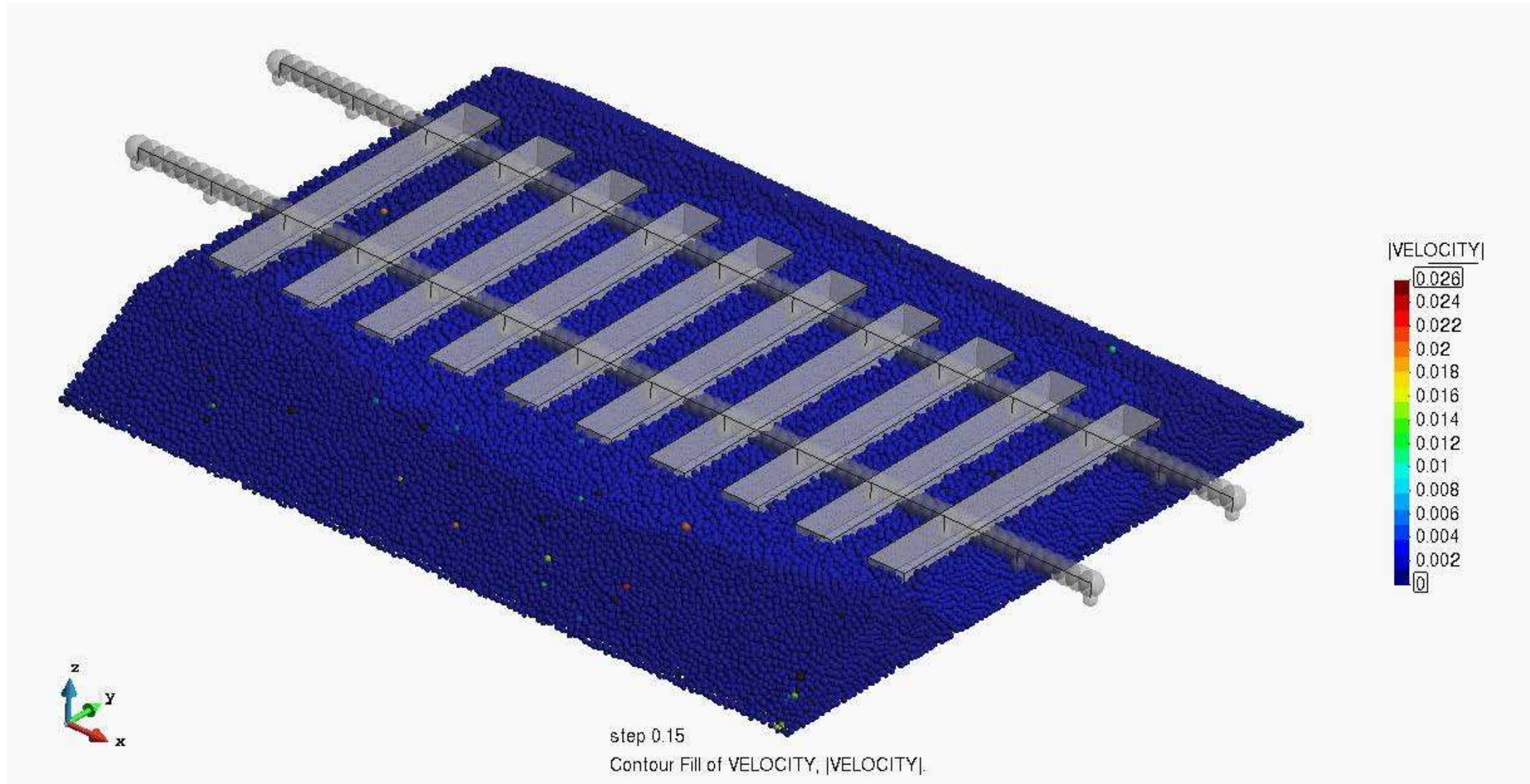
Radius of the curve

Rail cross section

Moment of inertia horizontal axis

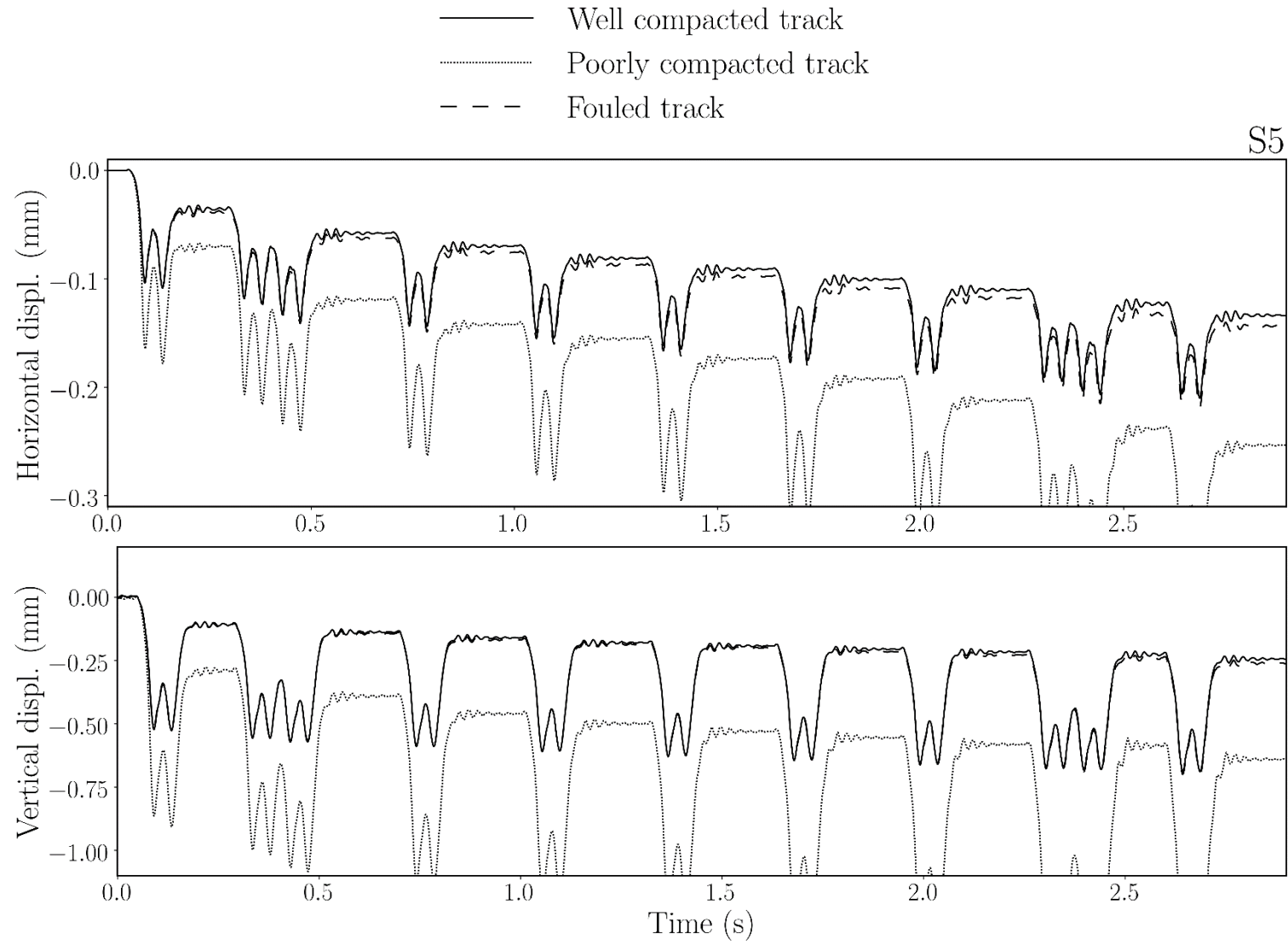
Moment of inertia vertical axis

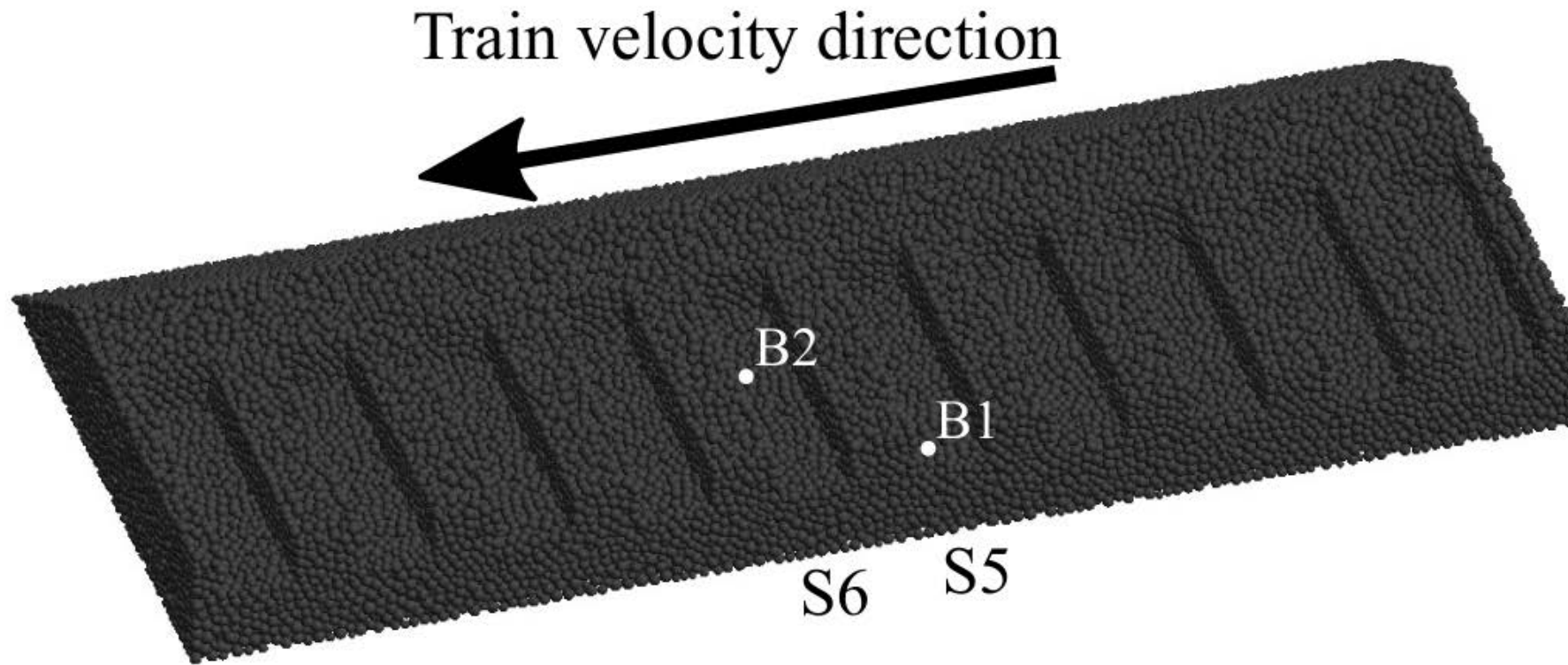




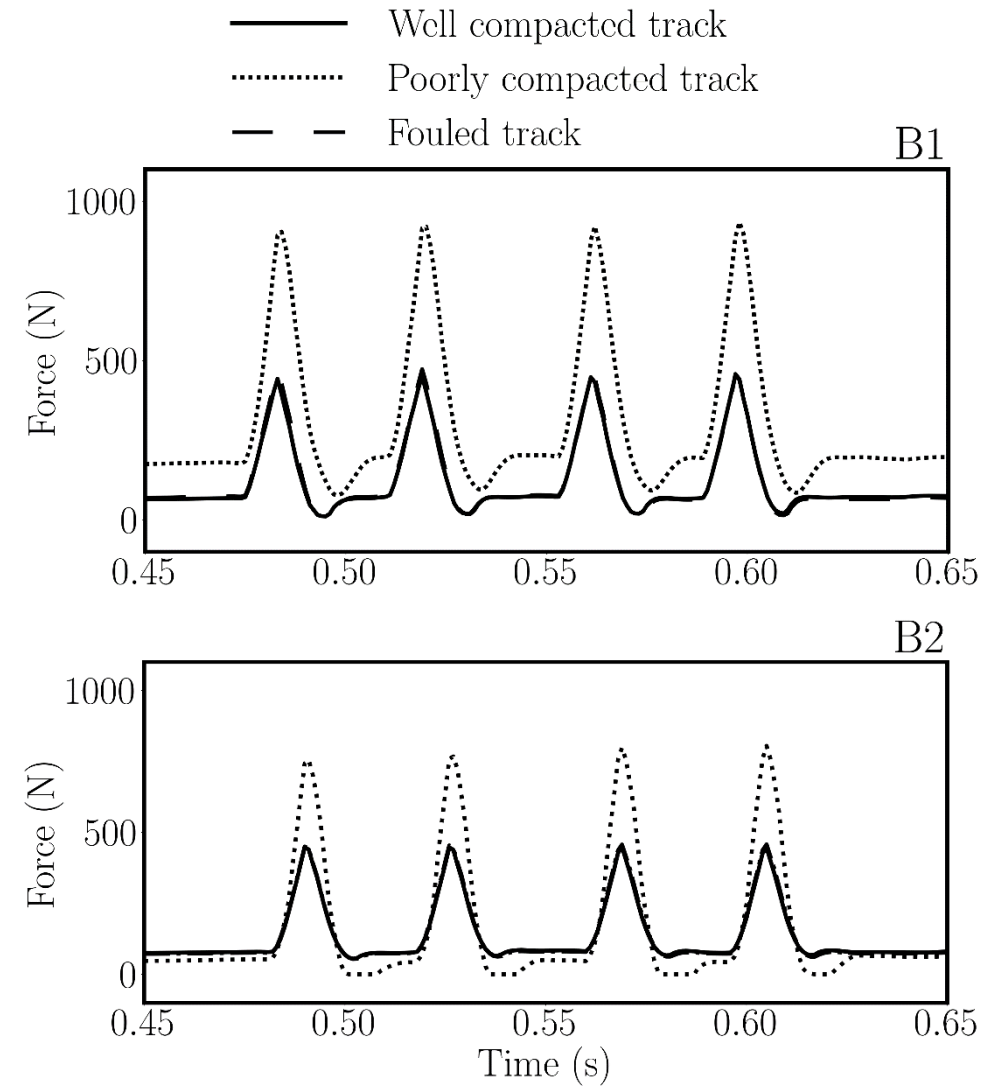
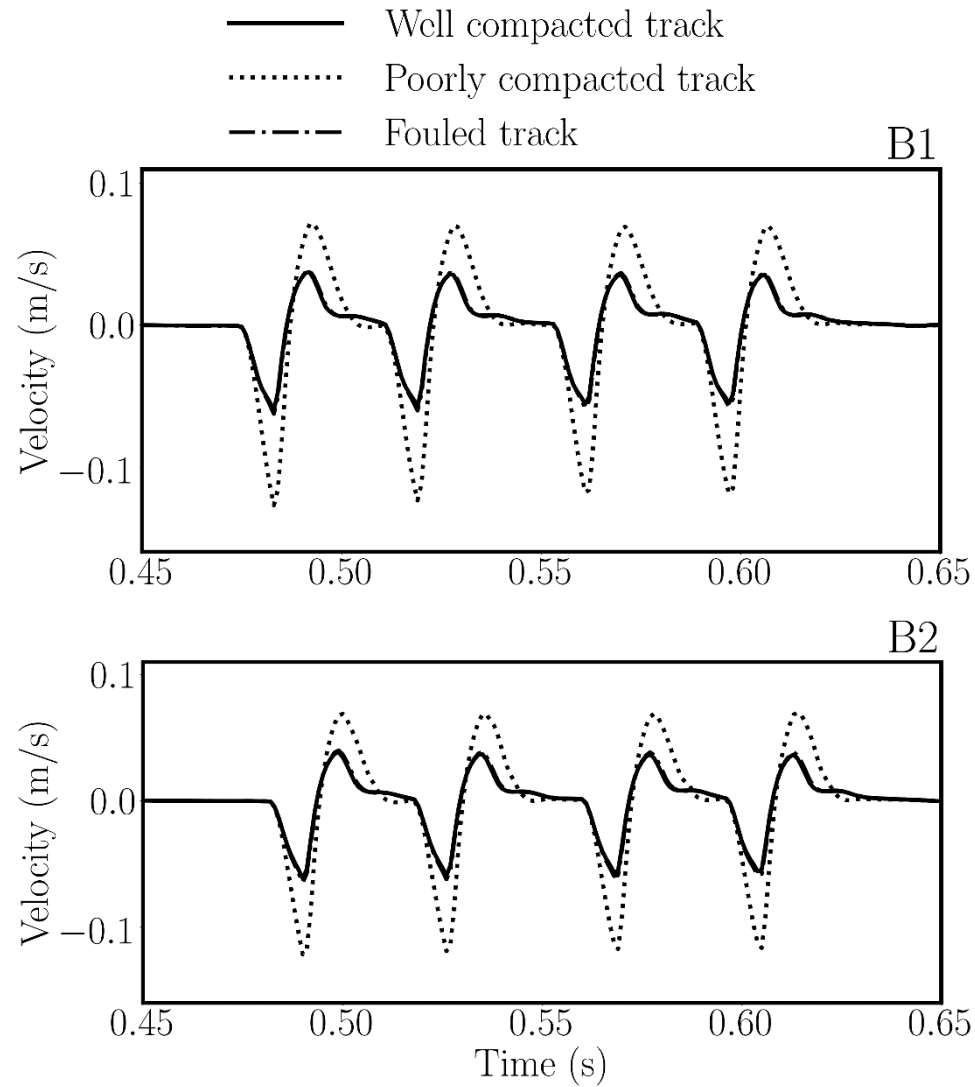
Ballast | Sleepers | Rails, bearing plates | Boundary walls | Subballast |  
**| Full scale railway track tests |** Summary and ongoing work











## **Summary and ongoing work**

- Spherical particles are useful for evaluating the macroscopic behaviour of the track (not valid, for example, to analyse the distribution of contacts)
- The DEM can accurately reproduce the behavior of rails and bearing plates making easy the coupling with railway ballast discrete particles
- The numerical tool presented allows the user to test different situations:
  - Ballast granulometry or properties
  - Sleepers design
  - Bearing plates and rails

## RESI LTRACK (Resilience of Railway Infrastructures Against Climate Change)



- Analysing how to measure track deflections in a real railway track section (high-speed if possible)
- Searching more data to validate conical damage parameters and ballast fouling conditions
- Testing other particle geometries (clusters of spheres) more similar to ballast particles

**Thank you for your attention!**

**Questions?**

jirazabal@cimne.upc.edu